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**NONRESIDENTIAL ACM MANUAL APPENDIX NA****Appendix NA - Nonresidential ACM Approval Application**

## CALIFORNIA ENERGY RESOURCES

## CONSERVATION AND DEVELOPMENT COMMISSION

APPLICATION FOR APPROVAL OF A VENDOR-CERTIFIED ALTERNATIVE CALCULATION METHOD FOR  
USE IN DEMONSTRATING COMPLIANCE WITH THE NONRESIDENTIAL BUILDING ENERGY EFFICIENCY  
STANDARDS PER SECTION 141, TITLE 24 OF THE CALIFORNIA CODE OF REGULATIONS

## Part I: General Information

1. Organization filing application:

Name: \_\_\_\_\_ Phone: (    ) \_\_\_\_\_

Address: \_\_\_\_\_

\_\_\_\_\_

2. Name of person responsible for completion of this application:

Name: \_\_\_\_\_ Phone: (    ) \_\_\_\_\_

Address: \_\_\_\_\_

\_\_\_\_\_

3. Name, Date, and Version of the Alternative Calculation Method (ACM):

Name: \_\_\_\_\_ Date: \_\_\_\_\_

Version: \_\_\_\_\_

4. Has a previous version of this ACM ever been certified?

☐ YES    ☐ NO

5. Has this ACM been previously submitted for approval or certification?

☐ YES    ☐ NO

6. Has this ACM ever been used to analyze the energy use of a building in California?

☐ YES    ☐ NO

7. Has this ACM ever been used to determine compliance with the energy efficiency standards of California?

☐ YES    ☐ NO

## VENDOR CERTIFICATION OF ALTERNATIVE CALCULATION METHOD

I/We, \_\_\_\_\_, certify that the alternative calculation method (ACM), herein  
name(s)  
designated \_\_\_\_\_, version \_\_\_\_\_, dated \_\_\_\_\_,  
name of alternative calculation method version last saved  
update  
occupying \_\_\_\_\_ bytes of memory, conforms to all of the requirements specified for an  
exact memory size in bytes

ACM for Commission approval listed in the Nonresidential ACM Approval Manual. I/We specifically certify that this ACM successfully conforms to the test criteria for each and every ACM capability test in Chapter 4 of the Alternative Calculation Method (ACM) Approval Manual for the Nonresidential building energy efficiency standards. Moreover, I/we certify that, to the best of my/our knowledge and belief, we have found no instances where this ACM would indicate compliance for a proposed building that the reference computer program using the reference method would indicate fails to comply with the building energy efficiency standards.

I/We also understand that all required inputs must be available in any approvable ACM but the ACM is not required to model the features described by a given set of inputs. I/We stipulate that this ACM gives the user access to the required inputs and that this ACM automatically warns the user when building inputs use features that the ACM cannot model with sufficient accuracy and automatically fails the proposed building by a margin sufficient to meet the test criteria for any test of that capability.

Signed:

Date:

**ACM Application Test Results for  
Required Capabilities Tests**

TEST	PTa	STa	DTa	PTr	STr	DTr	CR1	CR2	LITEr	RECPa	CR3	CR4
A11A09												
A12A09												
A13A09												
A21B13												
A22B13												
A23B06												
A24B16												
A25B03												
A26B13												
A27B16												
B11B13												
B12B13												
B13B13												
B14B06												
B15B16												
B21B12												
B22B12												
B23B12												

$DT_i = PT_i - ST_i$  where  $i$  is either 'a' for acm or 'r' for reference

$CR1 = DT_a - (0.85 \times DTr - 1) > 0$  when  $DT_a \geq 0$

$CR3 = LITE_a / LITE_r$  must be  $\geq 0.980$  and  $\leq 1.020$

$CR2 = DT_a - (1.15 \times DTr - 1) > 0$  when  $DT_a < 0$

$CR4 = RECP_a / RECP_r$  must be  $\geq 0.980$  and  $\leq 1.020$

**ACM Application Test Results for  
Required Capabilities Tests**

TEST	PTa	STa	DTa	PTr	STr	DTr	CR1	CR2	LITEr	RECP <sub>r</sub>	CR3	CR4
B24B03												
B31D12												
B32D12												
C11A10												
C12A10												
C13A10												
C14A10												
C15A10												
C21B10												
C22C16												
D11D12												
D12D12												
D13D07												
D14D07												
E11D16												
E12D16												
E13D16												
E14D14												

$DT_i = PT_i - ST_i$  where  $i$  is either 'a' for acm or 'r' for reference

$CR1 = DT_a - (0.85 \times DTr - 1) > 0$  when  $DT_a \geq 0$

$CR3 = LITE_a / LITE_r$  must be  $\geq 0.980$  and  $\leq 1.020$

$CR2 = DT_a - (1.15 \times DTr - 1) > 0$  when  $DT_a < 0$

$CR4 = RECP_a / RECP_r$  must be  $\geq 0.980$  and  $\leq 1.020$

**ACM Application Test Results for  
Required Capabilities Tests**

TEST	PTa	STa	DTa	PTr	STr	DTr	CR1	CR2	LITEr	RECPa	CR3	CR4
E15D14												
E16D14												
E21B16												
E22B16												
E23B16												
E24B12												
E25B12												
E26B12												
F11A07												
F12A13												
F13B12												
F14B12												
F15A01												
G11A11												
G12A11												
G13A11												
G14A11												
G15B03												
G16B16												

$DT_i = PT_i - ST_i$  where  $i$  is either 'a' for acm or 'r' for reference

$CR1 = DT_a - (0.85 \times DTr - 1) > 0$  when  $DT_a \geq 0$

$CR3 = LITE_a / LITE_r$  must be  $\geq 0.980$  and  $\leq 1.020$

$CR2 = DT_a - (1.15 \times DTr - 1) > 0$  when  $DT_a < 0$

$CR4 = RECP_a / RECP_r$  must be  $\geq 0.980$  and  $\leq 1.020$

**ACM Application Test Results for  
Optional Capabilities Tests**

TEST	PTa	STa	DTa	PTr	STr	DTr	CR1	CR2	LITEr	RECPr	CR3	CR4
OC1A09												
O11B13												
O12B13												
O21B13												
O22B13												
O23B13												
O24B13												
O31A12												
O32A12												
O33A12												
O41B13												
O61B12												
O62B12												
O63B12												
O64B12												
O65B12												
O66B12												

$DT_i = PT_i - ST_i$  where  $i$  is either 'a' for acm or 'r' for reference

$CR1 = DT_a - (0.85 \times DTr - 1) > 0$  when  $DT_a \geq 0$

$CR3 = LITE_a / LITE_r$  must be  $\geq 0.980$  and  $\leq 1.020$

$CR2 = DT_a - (1.15 \times DTr - 1) > 0$  when  $DT_a < 0$

$CR4 = RECP_a / RECPr$  must be  $\geq 0.980$  and  $\leq 1.020$



**ACM Application Test Results for  
Optional Capabilities Tests**

TEST	PTa	STa	DTa	PTr	STr	DTr	CR1	CR2	LITEr	RECPr	CR3	CR4
O71B12												
O81A11												
O82A15												
O91A13												
O92A11												
O93A12												
O94A13												

$DT_i = PT_i - ST_i$  where  $i$  is either 'a' for acm or 'r' for reference

$CR1 = DT_a - (0.85 \times DTr - 1) > 0$  when  $DT_a \geq 0$

$CR3 = LITE_a / LITE_r$  must be  $\geq 0.980$  and  $\leq 1.020$

$CR2 = DT_a - (1.15 \times DTr - 1) > 0$  when  $DT_a < 0$

$CR4 = RECP_a / RECPr$  must be  $\geq 0.980$  and  $\leq 1.020$

## **NONRESIDENTIAL ACM MANUAL APPENDIX NB**

### **Appendix NB - Illuminance Categories and Luminaire Power**

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#### ***Illuminance Categories***

Please see Chapter 10 in the IESNA Lighting Handbook, Ninth Edition.

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#### ***Illuminance Categories and Luminaire Power***

Luminaire power shall be taken from the following tables.

Table NB-1 – Fluorescent Circline

Table NB-2 – Compact Fluorescent 2D

Table NB-3 – Compact Fluorescent

Table NB-4 – Long Compact Fluorescent

Table NB-5 – Fluorescent U-Tubes

Table NB-6 – Fluorescent Linear Lamps – Preheat

Table NB-7 – Fluorescent Linear Lamps T5

Table NB-8 – Fluorescent Rapid Start T-8

Table NB-9 – Fluorescent Rapid Start T-12

Table NB-10 – Fluorescent Rapid Start High Output (HO) T8 & T12, 8 ft

Table NB-11 – Fluorescent Instant Start (single pin base "Slimline") T12, 4 ft

Table NB-12 – Fluorescent Instant Start (single pin base "Slimline") T8 & T12, 8 ft.

Table NB-13 – High Intensity Discharge

Table NB-14 – 12 Volt Tungsten Halogen Lamps Including MR16, Bi-pin, AR70, AR111, PAR36

Table NB-1 – Fluorescent Circline

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
Rapid Start (22 W)	1	FC8T9	1	MAG STAND.	Mag. Stand.	27	8" OD
T5 Program Start (22 W)	1	FC9T5	1	ELECT NO	Electronic Normal Light	28	8" OD
	2	FC9T5	1	ELECT NO	Electronic Normal Light	53	
T5 Program Start (40 W)	1	FC12T5	1	ELECT NO	Electronic Normal Light	41	12" OD
	2	FC12T5	1	ELECT NO	Electronic Normal Light	80	
T5 Rapid Start (55 W)	1	FC12T5HO	1	ELECT NO	Electronic Normal Light	55	12" OD
	2	FC12Tag5HO	1	ELECT NO	Electronic Normal Light	103	
	1	FC12T5HO	1	ELECT DIM	Electronic Dimming	12-59	
	2	FC12T5HO	1	ELECT DIM	Electronic Dimming	24-114	
T5 Rapid Start (40 + 22 W)	1+1	FC12T5/FC9T5	1	ELECT NO	Electronic Normal Light	68	8" & 12" OD

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-2 – Compact Fluorescent 2D

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
10W, GR10q-4 Four Pin Base	1	CFS10W/GR10q	1	MAG STD	Mag. Stand.	16	3.6" across
	1	CFS10W/GR10q	1	ELECT	Electronic	13	
	2	CFS10W/GR10q	1	ELECT	Electronic	26	
16W, GR10q-4 Four Pin Base	1	CFS16W/GR10q	1	MAG STD	Mag. Stand.	23	5.5" across
	1	CFS16W/GR10q	1	ELECT	Electronic	15	
	2	CFS16W/GR10q	1	ELECT	Electronic	30	
21W, GR10q-4 Four Pin Base	1	CFS21W/GR10q	1	MAG STD	Mag. Stand.	31	5.5" across
	1	CFS21W/GR10q	1	ELECT	Electronic	21	
	2	CFS21W/GR10q	1	ELECT	Electronic	42	
28W, GR10q-4 Four Pin Base	1	CFS28W/GR10q	1	MAG STD	Mag. Stand.	38	8.1" across
	1	CFS28W/GR10q	1	ELECT	Electronic	28	
	2	CFS28W/GR10q	1	ELECT	Electronic	56	
(38W, GR10q-4 Four Pin Base	1	CFS38W/GR10q	1	ELECT	Electronic	37	8.1" across
	2	CFS38W/GR10q	1	ELECT	Electronic	74	

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-3 – Compact Fluorescent

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
Twin (5 W, G23 Two Pin Base - F5TT Lamp)	1	CFT5W/G23	1	MAG STD	Mag. Stand.	9	4.1" MOL
	2	CFT5W/G23	2	MAG STD	Mag. Stand.	18	
Twin (7 W, G23 Two Pin Base - F7TT Lamp)	1	CFT7W/G23	1	MAG STD	Mag. Stand.	11	5.3" MOL
	2	CFT7W/G23	2	MAG STD	Mag. Stand.	22	
Twin (7 W, 2G7 Four Pin Base - F7TT Lamp)	1	CFT7W/2G7	1	ELECT	Electronic	8	5.3" MOL
	2	CFT7W/2G7	2	ELECT	Electronic	16	
Twin (9 W, G23 Two Pin Base - F9TT Lamp)	1	CFT9W/G23	1	MAG STD	Mag. Stand.	13	6.5" MOL
	2	CFT9W/G23	2	MAG STD	Mag. Stand.	26	
Twin (9 W, 2G7 Four Pin Base - F9TT Lamp)	1	CFT9W/2G7	1	ELECT	Electronic	10	6.5" MOL
	2	CFT9W/2G7	2	ELECT	Electronic	20	
Twin (13 W, GX23 Two Pin Base - F13TT)	1	CFT13W/GX23	1	MAG STD	Mag. Stand.	17	7.5" MOL
	2	CFT13W/GX23	2	MAG STD	Mag. Stand.	34	
Twin (13 W, 2GX7 Four Pin Base - F13TT)	1	CFT13W/2GX7	1	ELECT	Electronic	17	7.5" MOL
	2	CFT13W/2GX7	2	ELECT	Electronic	34	
Quad (9 W, G23-2 Two Pin Base - F9DTT Lamp)	1	CFQ9W/G23-2	1	MAG STD 120	120 V Mag. Stand.	13	4.4" MOL
	2	CFQ9W/G23-2	2	MAG STD 120	120 V Mag. Stand.	26	
Quad (13 W, G24d-1 Two Pin Base - F13DTT Lamp)	1	CFQ13W/G24d -1	1	MAG STD 120	120 V Mag. Stand.	18	6.0" MOL
	2	CFQ13W/G24d -1	2	MAG STD 120	120 V Mag. Stand.	36	
	1	CFQ13W/G24d -1	1	MAG STD 277	277 V Mag. Stand.	16	
	2	CFQ13W/G24d -1	2	MAG STD 277	227 V Mag. Stand.	32	
Quad (13 W, GX23-2 Two Pin Base)	1	CFQ13W/GX2 3-2	1	MAG STD	Mag. Stand.	17	4.8" MOL
	2	CFQ13W/GX2 3-2	2	MAG STD	Mag. Stand.	34	
Quad (16W GX32d-1 Two Pin Base)	1	CFQ16W/GX3 2d-1	1	MAG STD	Mag. Stand.	20	5.5" MOL
	2	CFQ16W/GX3 2d-1	2	MAG STD	Mag. Stand.	40	
Quad (18 W, G24d-2 Two Pin Base - F18DTT Lamp)	1	CFQ18W/G24d -2	1	MAG STD 120	120 V Mag. Stand.	25	6.8" MOL
	2	CFQ18W/G24d -2	2	MAG STD 120	120 V Mag. Stand.	50	
	1	CFQ18W/G24d -2	1	MAG STD 277	227 V Mag. Stand.	22	

Type	Lamps		Ballasts		System Watts	Comment
	Number	Designation	Number	Designation Description		
	2	CFQ18W/G24d -2	2	MAG STD 277 227 V Mag. Stand.	44	
	1	CFQ22W/GX3 2d-2	1	MAG STD Mag. Stand.	27	6.0" MOL
Quad (22W, GX32d Two Pin Base)	2	CFQ22W/GX3 2d-2	2	MAG STD Mag. Stand.	54	
Quad (26 W, G24d-3 Two Pin Base - F26DTT Lamp)	1	CFQ26W/G24d -3	1	MAG STD 120 120 V Mag. Stand.	37	7.6" MOL
	2	CFQ26W/G24d -3	2	MAG STD 120 120 V Mag. Stand.	74	
	1	CFQ26W/G24d -3	1	MAG STD 277 227 V Mag. Stand.	33	
	2	CFQ26W/G24d -3	2	MAG STD 277 227 V Mag. Stand.	66	
	1	CFQ26W/G24d -3	1	ELECT 277V 277 V Electronic	27	
	2	CFQ26W/G24d -3	2	ELECT 277V 277 V Electronic	54	
Quad (28W GX32d Two Pin Base)	1	CFQ28W/GX3 2d-3	1	MAG STD Mag. Stand.	34	6.8" MOL
	2	CFQ28W/GX3 2d-3	2	MAG STD Mag. Stand.	68	
Quad (10 W, G24q-1 Four Pin Base)	1	CFQ10W/G24q -1	1	MAG STD 120 120 V Mag. Stand.	16	4.6" MOL
	2	CFQ10W/G24q -1	2	MAG STD 120 120 V Mag. Stand.	32	
	1	CFQ10W/G24q -1	1	MAG STD 277 227 V Mag. Stand.	13	
	2	CFQ10W/G24q -1	2	MAG STD 277 227 V Mag. Stand.	26	
Quad (13 W, G24q-1 Four Pin Base)	1	CFQ13W/G24q -1	1	MAG STD 120 120 V Mag. Stand.	18	6.0" MOL
	2	CFQ13W/G24q -1	2	MAG STD 120 120 V Mag. Stand.	36	
	1	CFQ13W/G24q -1	1	MAG STD 277 227 V Mag. Stand.	16	
	2	CFQ13W/G24q -1	2	MAG STD 277 227 V Mag. Stand.	32	
	1	CFQ13W/G24q -1	1	ELECT Electronic	14	
	2	CFQ13W/G24q -1	2	ELECT Electronic	25	
Quad (13 W, GX7 Four Pin Base)	1	CFQ13W/GX7	1	MAG STD Mag. Stand.	17	4.8" MOL
	2	CFQ13W/GX7	2	MAG STD Mag. Stand.	34	
Quad (18 W, G24q-2 Four Pin Base)	1	CFQ18W/G24q -2	1	MAG STD 120 120 V Mag. Stand.	25	6.8" MOL

Type	Lamps		Ballasts		System Watts	Comment
	Number	Designation	Number	Designation Description		
	2	CFQ18W/G24q-2	2	MAG STD 120 120 V Mag. Stand.	50	
	1	CFQ18W/G24q-2	1	MAG STD 277 227 V Mag. Stand.	22	
	2	CFQ18W/G24q-2	2	MAG STD 277 227 V Mag. Stand.	44	
	1	CFQ18W/G24q-2	1	ELECT Electronic	21	
	2	CFQ18W/G24q-2	2	ELECT Electronic	38	
Triple (13 W, GX24q-1 Four Pin Base)	1	CFM 13W/GX24q-1	1	MAG STD Mag. Stand.	18	4.2" MOL
	2	CFM 13W/GX24q-1	2	MAG STD Mag. Stand.	36	
	1	CFM 13W/GX24q-1	1	ELECT Electronic	14	
	2	CFM 13W/GX24q-1	2	ELECT Electronic	25	
Triple (18W, GX24q-2 Four Pin Base)	1	CFM 18W/GX24q-2	1	MAG STD Mag. Stand.	25	5.0" MOL
	2	CFM 18W/GX24q-2	2	MAG STD Mag. Stand.	50	
	1	CFM 18W/GX24q-2	1	ELECT Electronic	21	
	2	CFM 18W/GX24q-2	2	ELECT Electronic	38	
Triple (26W, GX24q-3 Four Pin Base)	1	CFTR 26W/GX24q-3	1	MAG STD Mag. Stand.	37	4.9 to 5.4" MOL
	2	CFTR 26W/GX24q-3	2	MAG STD Mag. Stand.	74	
	1	CFTR 26W/GX24q-3	1	ELECT Electronic	28	
	2	CFTR 26W/GX24q-3	1	ELECT Electronic	55	
	1	CFTR 26W/GX24q-3	1	ELECT DIM Electronic Dimming	8~29	BF .05~1.0
	2	CFTR 26W/GX24q-3	1	ELECT DIM Electronic Dimming	12~57	BF .05~1.0
Triple (32 W, GX24q-3 Four Pin Base)	1	CFTR32WGX2 4q-3	1	ELECT Electronic	35	
	2	CFTR32WGX2 4q-3	1	ELECT Electronic	69	
	1	CFTR32WGX2 4q-3	1	ELECT DIM Electronic Dimming	9~38	BF .05~1.05
	2	CFTR32WGX2 4q-3	1	ELECT DIM Electronic Dimming	20~76	BF .05~1.05

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
Triple or Quad (42W, GX24q-4 Four Pin Base)	1	CFTR42WGX2 4q-4	1	ELECT	Electronic	46	
	2	CFTR42WGX2 4q-4	1	ELECT	Electronic	94	
	1	CFTR42WGX2 4q-4	1	ELECT DIM	Electronic Dimming	10~49	BF .05~1.05
	2	CFTR42WGX2 4q-4	1	ELECT DIM	Electronic Dimming	20~98	BF .05~1.05
Triple or Quad (57W, GX24q-5 Four Pin Base)	1	CFTR57WGX2 4q-5	1	ELECT	Electronic	62	
	1	CFTR57WGX2 4q-5	1	ELECT DIM	Electronic Dimming	18~66	BF .05~1.05
Triple or Quad (70W, GX24q-6 Four Pin Base)	1	CFTR70WGX2 4q-6	1	ELECT	Electronic	75	
	1	CFTR70WGX2 4q-6	1	ELECT DIM	Electronic Dimming	18~80	BF .05~1.00

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-4 –Long Compact Fluorescent

Type	Lamps		Ballasts		System Watts	Comment
	Number	Designation	Number	Description		
T5 Twin (18W - F18TT Lamp)	1	FT18W/2G11	1	MAG.	Mag. Energy Efficient	23 BF~1.0
	2	FT18W/2G11	1	MAG.	Mag. Energy Efficient	46 BF~1.0
	3	FT18W/2G11	1	MAG.	Mag. Energy Efficient	69
	1	FT18W/2G11	1	ELECT	Electronic	24
	2	FT18W/2G11	1	ELECT	Electronic	35
	3	FT18W/2G11	1	ELECT	Electronic	52
T5 Twin (24-27W- F24TT or F27TT Lamp)	1	FT24W/2G11	1	MAG.	Mag. Energy Efficient	32
	2	FT24W/2G11	1	MAG.	Mag. Energy Efficient	66
	3	FT24W/2G11	1	MAG.	Mag. Energy Efficient	98
	1	FT24W/2G11	1	ELECT	Electronic	27 BF~1.0
	2	FT24W/2G11	1	ELECT	Electronic	52 BF~1.0
T5 Twin (36-39W - F36TT or F39TT Lamp)	1	FT36W/2G11	1	MAG.	Mag. Energy Efficient	51
	2	FT36W/2G11	1	MAG.	Mag. Energy Efficient	66
	3	FT36W/2G11	2	MAG.	Mag. Energy Efficient	117
	1	FT36W/2G11	1	ELECT	Electronic	37
	2	FT36W/2G11	1	ELECT	Electronic	70
	1	FT36W/2G11	1	ELECTHO	Electronic High Output	46 BF=1.22
	2	FT36W/2G11	1	ELECTHO	Electronic High Output	86 BF=1.20
T5 Twin (40 W - F40TT Lamp)	1	FT40W/2G11	1	MAG.	Mag. Energy Efficient	43
	2	FT40W/2G11	1	MAG.	Mag. Energy Efficient	86
	3	FT40W/2G11	2	MAG.	Mag. Energy Efficient	130
Electronic Ballasts	1	FT40W/2G11	1	ELECT NO	Electronic	41 BF~.90
	2	FT40W/2G11	1	ELECT NO1	Electronic	72 BF~.88
	2	FT40W/2G11	1	ELECT NO2	Electronic	78 BF~.97
	3	FT40W/2G11	1	ELECT NO	Electronic	103 BF~.86
	1	FT40W/2G11	1	ELECT HO	Electronic High Output	50 BF ~ 1.1
	1	FT40W/2G11	1	ELECT DIM1	Electronic Dimming	10-41 BF .05~1.0
	2	FT40W/2G11	1	ELECT DIM1	Electronic Dimming	17-80 BF .05~1.0
	1	FT40W/2G11	1	ELECT DIM2	Electronic Dimming	11-38 BF .05~.88
	2	FT40W/2G11	1	ELECT DIM2	Electronic Dimming	16-76 BF .05~.88
T5 Twin (50 W - F50TT Lamp)	1	FT50W/2G11	1	ELECT NO	Electronic Normal Output	54 BF~.98
	2	FT50W/2G11	1	ELECT NO	Electronic Normal Output	106 BF~.98
	1	FT50W/2G11	1	ELECT HO	Electronic High Output	61 BF~1.12
	2	FT50W/2G11	1	ELECT HO	Electronic High Output	115 BF~1.10
	1	FT50W/2G11	1	ELECT DIM	Electronic Dimming	51



Type	Lamps		Ballasts		System Watts	Comment
	Number	Designation	Number	Designation	Description	
	2	FT50W/2G11	1	ELECT DIM	Electronic Dimming	92
T5 Twin (55 W - F55TT Lamp)	1	FT55W/2G11	1	ELECT NO	Electronic Normal Output	58 BF~.92
	2	FT55W/2G11	1	ELECT NO	Electronic Normal Output	109 BF~.90
	1	FT55W/2G11	1	ELECT DIM	Electronic Dimming	13-59 BF .03~.90
	2	FT55W/2G11	1	ELECT DIM	Electronic Dimming	24-114 BF .03~.90
T5 Twin (80 W – F80TT Lamp)	1	FT80W/2G11	1	ELECT NO	Electronic	91 BF~1.00

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-5 – Fluorescent U-Tubes

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
2 ft. Fluorescent U-Tube T8 (32W - FBO31T8 or F32T8/U/6 Lamp)	1	FB31T8/F32T8U	0.5	MAG.	Mag. Energy Efficient	35	Tandem wired
	1	FB31T8/F32T8U	1	MAG.	Mag. Energy Efficient	36	
	2	FB31T8/F32T8U	1	MAG.	Mag. Energy Efficient	69	
	3	FB31T8/F32T8U	1.5	MAG.	Mag. Energy Efficient	104	Tandem wired
	3	FB31T8/F32T8U	2	MAG.	Mag. Energy Efficient	105	
	1	FB31T8/F32T8U	1	ELECT NO	Electronic Normal Output	39	
	2	FB31T8/F32T8U	1	ELECT NO	Electronic Normal Output	62	
	3	FB31T8/F32T8U	1	ELECT NO	Electronic Normal Output	92	
	4	FB31T8/F32T8U	1	ELECT NO	Electronic Normal Output		
	1	FB31T8/F32T8U	1	ELECT DIM	Electronic Dimming	9~33	BF .05~.88
	2	FB31T8/F32T8U	1	ELECT DIM	Electronic Dimming	14~64	BF .05~.88
	3	FB31T8/F32T8U	1	ELECT DIM	Electronic Dimming	18~93	BF .05~.88
	4	FB31T8/F32T8U	1	ELECT DIM	Electronic Dimming	25~116	BF .05~.88
2 ft. Fluorescent U-Tube T12 ("Energy Saving" 34W)	1	FB40T12/ES	0.5	MAG.	Mag. Energy Efficient	36	Tandem wired
	1	FB40T12/ES	1	MAG.	Mag. Energy Efficient	43	
	2	FB40T12/ES	1	MAG.	Mag. Energy Efficient	72	
	3	FB40T12/ES	1	MAG.	Mag. Energy Efficient	105	
	3	FB40T12/ES	1.5	MAG.	Mag. Energy Efficient	108	Tandem wired
	3	FB40T12/ES	2	MAG.	Mag. Energy Efficient	115	
	1	FB40T12/ES	0.5	ELECT	Electronic	30	Tandem wired
	1	FB40T12/ES	1	ELECT	Electronic	31	
	2	FB40T12/ES	1	ELECT	Electronic	59	
	3	FB40T12/ES	1	ELECT	Electronic	90	
	3	FB40T12/ES	1.5	ELECT	Electronic	88	Tandem wired
	3	FB40T12/ES	2	ELECT	Electronic	90	

RO = ballast factor 70 to 85%

NO = ballast factor 85 to 100%

HO = ballast factor &gt;100%

Table NB-6 – Fluorescent Linear Lamps – Preheat

Type	Lamps		Ballasts			System Watts	Comment
	Nmbr	Designation	Nmbr	Designation	Description		
Fluorescent Preheat T5 (8W)	1	F8T5	1	MAG STD	Mag. Stand.	12	12" MOL
Fluorescent Preheat T8 (15W)	1	F15T8	1	MAG STD	Mag. Stand.	19	18" MOL
Fluorescent Preheat T12 (15W)	1	F15T12	1	MAG STD	Mag. Stand.	19	18" MOL
Fluorescent Preheat T12 (20W)	1	F20T12	1	MAG STD	Mag. Stand.	25	24" MOL
	2	F20T12	1	MAG STD	Mag. Stand.	50	24" MOL
Fluorescent Preheat T8 (30W)	1	F30T8	1	MAG STD	Mag. Stand.	46	30" MOL
	2	F30T8	1	MAG STD	Mag. Stand.	79	30" MOL

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-7 – Fluorescent Linear Lamps T5

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
~23" Fluorescent Program Start T5 (14W)	1	F14T5	1	ELECT	Elect. Program Start BF=1	18	
	2	F14T5	1	ELECT	Elect. Program Start BF=1	34	
~34.5" Fluorescent Program Start T5 (21W)	1	F21T5	1	ELECT	Elect. Program Start BF=1	27	
	2	F21T5	1	ELECT	Elect. Program Start BF=1	50	
~46" Fluorescent Program Start T5 (28W)	1	F28T5	1	ELECT	Elect. Program Start BF=1	30	
	2	F28T5	1	ELECT	Elect. Program Start BF=1	60	
~58.5" Fluorescent Program Start T5 (35W)	1	F35T5	1	ELECT	Elect. Program Start BF=1	40	
	2	F35T5	1	ELECT	Elect. Program Start BF=1	78	
~23" Fluorescent Program Start T5 High Output (24W)	1	F24T5HO	1	ELECT	Elect. Program Start BF=1	27	
	2	F24T5HO	1	ELECT	Elect. Program Start BF=1	52	
~34.5" Fluorescent Program Start T5 High Output (39W)	1	F39T5	1	ELECT	Elect. Program Start BF=1	43	
	2	F39T5	1	ELECT	Elect. Program Start BF=1	85	
~46" Fluorescent Program Start T5 High Output (54W)	1	F54T5	1	ELECT	Elect. Program Start BF=1	62	
	2	F54T5	1	ELECT	Elect. Program Start BF=1	117	

	1	F54T5	1	ELECT DIM	Elect. Dimming	12-63
	2	F54T5	1	ELECT DIM	Elect. Dimming	24-125
~57.5" Fluorescent Program Start T5 High Output (80W)	1	°F80T5	1	ELECT	Elect. Program Start BF=1	89
RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%						

Table NB-8 – Fluorescent Rapid Start T-8

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
2 foot Fluorescent Rapid Start T8 (17W)	1	F17T8	1	MAG.	Mag. Energy Efficient	24	
	2	F17T8	1	MAG.	Mag. Energy Efficient	45	
Electronic Ballasts	1	F17T8	1	ELECT NO	Electronic Normal Output	22	
	2	F17T8	1	ELECT NO	Electronic Normal Output	33	
	3	F17T8	1	ELECT NO	Electronic Normal Output	53	
	3	F17T8	2	ELECT NO	Electronic Normal Output	55	
	4	F17T8	1	ELECT NO	Electronic Normal Output	63	
2 foot Fluorescent Rapid Start T8 (17W)	1	F17T8	1	ELECT DIM	Electronic Dimming	8~20	BF .05~.88
	2	F17T8	1	ELECT DIM	Electronic Dimming	10~37	BF .05~.88
	3	F17T8	1	ELECT DIM	Electronic Dimming	12~56	BF .05~.88
	4	F17T8	1	ELECT DIM	Electronic Dimming	18~69	BF .05~.88
3 foot Fluorescent Rapid Start T8 (25W)	1	F25T8	1	MAG.	Mag. Energy Efficient	33	
	2	F25T8	1	MAG.	Mag. Energy Efficient	65	
Electronic Ballasts	1	F25T8	1	ELECT NO	Electronic Normal Output	27	
	2	F25T8	1	ELECT NO	Electronic Normal Output	48	
	3	F25T8	1	ELECT NO	Electronic Normal Output	68	
	4	F25T8	1	ELECT NO	Electronic Normal Output	89	
	1	F25T8	1	ELECT RO	Electronic Reduced Output	24	
	2	F25T8	1	ELECT RO	Electronic Reduced Output	41	
	3	F25T8	1	ELECT RO	Electronic Reduced Output	59	
	4	F25T8	1	ELECT RO	Electronic Reduced Output	76	
	1	F25T8	1	ELECT HO	Electronic High Output	29	BF~1.05
	2	F25T8	1	ELECT HO	Electronic High Output	51	BF~1.05
	3	F25T8	1	ELECT HO	Electronic High Output	74	BF~1.05
	1	F25T8	1	ELECT DIM	Electronic Dimming	8~25	BF .05~.94
	2	F25T8	1	ELECT DIM	Electronic Dimming	13~49	BF .05~.94
	3	F25T8	1	ELECT DIM	Electronic Dimming	16~76	BF .05~.94

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
4 foot Fluorescent Rapid Start T12 for T-8 ballasts ("Energy Saving" 25W)	4	F25T8	1	ELECT DIM	Electronic Dimming	22~96	BF .05~.88
	1	F25T12ES	1	ELECT NO	Electronic Normal Output	27	
	2	F25T12ES	1	ELECT NO	Electronic Normal Output	52	
	3	F25T12ES	1	ELECT NO	Electronic Normal Output	77	
	4	F25T12ES	1	ELECT NO	Electronic Normal Output	95	
4 foot Fluorescent Instant Start T8 ("Energy Saving" 30W)	1	F32T8/30ES	1	ELECT NO	Electronic Normal Output	29	
	2	F32T8/30ES	1	ELECT NO	Electronic Normal Output	54	
	3	F32T8/30ES	1	ELECT NO	Electronic Normal Output	79	
	4	F32T8/30ES	1	ELECT NO	Electronic Normal Output	104	
	1	F32T8/30ES	1	ELECT RO	Electronic Reduced Output	27	
	2	F32T8/30ES	1	ELECT RO	Electronic Reduced Output	48	
	3	F32T8/30ES	1	ELECT RO	Electronic Reduced Output	70	
	4	F32T8/30ES	1	ELECT RO	Electronic Reduced Output	91	
	1	F32T8/30ES	1	ELECT NO EE	EE Normal Output	33	
	2	F32T8/30ES	1	ELECT NO EE	Energy efficiency Normal Output	52	
	3	F32T8/30ES	1	ELECT NO EE	Energy efficiency Normal Output	77	
	4	F32T8/30ES	1	ELECT NO EE	Energy efficiency Normal Output	101	
	1	F32T8/30ES	1	ELECT RO EE	EE Reduced Output	28	
	2	F32T8/30ES	1	ELECT RO EE	EE Reduced Output	45	
	3	F32T8/30ES	1	ELECT RO EE	EE Reduced Output	66	
	4	F32T8/30ES	1	ELECT RO EE	EE Reduced Output	88	
	1	F32T8	0.5	MAG.	Mag. Energy Efficient	35	Tandem wired
	1	F32T8	1	MAG.	Mag. Energy Efficient	39	
	2	F32T8	1	MAG.	Mag. Energy Efficient	70	

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
	3	F32T8	1.5	MAG.	Mag. Energy Efficient	105	Tandem wired
	3	F32T8	2	MAG.	Mag. Energy Efficient	109	
	4	F32T8	2	MAG.	Mag. Energy Efficient	140	(2) two-lamp ballasts
4 foot Fluorescent Rapid Start T8 (32W)	1	F32T8	1	ELECT NO	Electronic Normal Output	32	
	2	F32T8	1	ELECT NO	Electronic Normal Output	62	
	3	F32T8	1	ELECT NO	Electronic Normal Output	93	
	4	F32T8	1	ELECT NO	Electronic Normal Output	114	
	1	F32T8	1	EE NO	EE Normal Output	35	
	2	F32T8	1	EE NO	EE Normal Output	55	
	3	F32T8	1	EE NO	EE Normal Output	82	
	4	F32T8	1	EE NO	EE Normal Output	107	
	1	F32T8	1	ELECT RO	Electronic Reduced Output	29	
	2	F32T8	1	ELECT RO	Electronic Reduced Output	51	
	3	F32T8	1	ELECT RO	Electronic Reduced Output	76	
	4	F32T8	1	ELECT RO	Electronic Reduced Output	98	
	2	F32T8	1	ELECT HO	Electronic High Output	77	BF~1.13
	3	F32T8	1	ELECT HO	Electronic High Output	112	BF~1.18
	1	F32T8	1	EE RO	EE Reduced Output	30	
	2	F32T8	1	EE RO	EE Reduced Output	48	
	3	F32T8	1	EE RO	EE Reduced Output	73	
	4	F32T8	1	EE RO	EE Reduced Output	96	
	2	F32T8	1	ELECT TL	Electronic Two Level (50 & 100%)	65	
	1	F32T8	1	ELECT DIM1	Electronic Dimming	9~35	BF .05~1.0
	2	F32T8	1	ELECT DIM1	Electronic Dimming	15~68	BF .05~1.0
	3	F32T8	1	ELECT DIM1	Electronic Dimming	20~102	BF .05~1.0
	1	F32T8	1	ELECT DIM2	Electronic Dimming	9~33	BF .05~.88
	2	F32T8	1	ELECT DIM2	Electronic Dimming	14~64	BF .05~.88
	3	F32T8	1	ELECT DIM2	Electronic Dimming	18~93	BF .05~.88
	4	F32T8	1	ELECT DIM2	Electronic Dimming	25~116	BF .05~.88
5 foot Fluorescent	1	F40T8	1	MAG.	Mag. Energy Efficient	50	

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
Rapid Start T8 (40W)	2	F40T8	1	MAG.	Mag. Energy Efficient	92	
	1	F40T8	1	ELECT	Electronic	46	
	2	F40T8	1	ELECT	Electronic	79	
	3	F40T8	1	ELECT	Electronic	112	
3 foot Fluorescent Rapid Start T12 ("Energy-Saving" 25W)	1	F30T12/ES	1	MAG STD	Mag. Stand.	42	
	2	F30T12/ES	1	MAG STD	Mag. Stand.	74	
	3	F30T12/ES	1.5	MAG STD	Mag. Stand.	111	Tandem wired
	3	F30T12/ES	2	MAG STD	Mag. Stand.	116	
	2	F30T12/ES	1	MAG.	Mag. Energy Efficient	66	
	1	F30T12/ES	1	ELECT	Electronic	26	
	2	F30T12/ES	1	ELECT	Electronic	53	
3 foot Fluorescent Rapid Start T12 ("Stand." 30W)	1	F30T12	1	MAG STD	Mag. Stand.	46	
	2	F30T12	1	MAG STD	Mag. Stand.	79	
	3	F30T12	1.5	MAG STD	Mag. Stand.	118	Tandem wired
	3	F30T12	2	MAG STD	Mag. Stand.	125	
	2	F30T12	1	MAG.	Mag. Energy Efficient	73	
	1	F30T12	1	ELECT	Electronic	30	
	2	F30T12	1	ELECT	Electronic	60	
4 foot Fluorescent Rapid Start T12 ("Energy-Saving Plus" 32W)	1	F40T12/ES Plus	0.5	MAG.	Mag. Energy Efficient	34	Tandem wired
	1	F40T12/ES Plus	1	MAG.	Mag. Energy Efficient	41	
	2	F40T12/ES Plus	1	MAG.	Mag. Energy Efficient	68	
	3	F40T12/ES Plus	1	MAG.	Mag. Energy Efficient	99	
	3	F40T12/ES Plus	1.5	MAG.	Mag. Energy Efficient	102	Tandem wired
	3	F40T12/ES Plus	2	MAG.	Mag. Energy Efficient	109	
	4	F40T12/ES Plus	2	MAG.	Mag. Energy Efficient	136	(2) Two-lamp ballasts
RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%							



Table NB-9 – Fluorescent Rapid Start T-12

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
4 foot Fluorescent Rapid Start T12 ("Energy-Saving"34W)	1	F40T12/ES	0.5	MAG STD**	Mag. Stand.	42	Tandem wired
	1	F40T12/ES	1	MAG STD**	Mag. Stand.	48	
	2	F40T12/ES	1	MAG STD**	Mag. Stand.	82	
	3	F40T12/ES	1.5	MAG STD**	Mag. Stand.	122	Tandem wired
	3	F40T12/ES	2	MAG STD**	Mag. Stand.	130	
	4	F40T12/ES	2	MAG STD**	Mag. Stand.	164	(2) Two-lamp ballasts
	1	F40T12/ES	0.5	MAG.	Mag. Energy Efficient	36	Tandem wired
	1	F40T12/ES	1	MAG.	Mag. Energy Efficient	43	
	2	F40T12/ES	1	MAG.	Mag. Energy Efficient	72	
	3	F40T12/ES	1	MAG.	Mag. Energy Efficient	105	
	3	F40T12/ES	1.5	MAG.	Mag. Energy Efficient	108	Tandem wired
	3	F40T12/ES	2	MAG.	Mag. Energy Efficient	112	
	4	F40T12/ES	2	MAG.	Mag. Energy Efficient	144	(2) Two-lamp ballasts
	2	F40T12/ES	1	MAG HC	Mag. Heater Cutout	58	
	3	F40T12/ES	1.5	MAG HC	Mag. Heater Cutout	87	Tandem wired
	4	F40T12/ES	2	MAG HC	Mag. Heater Cutout	116	(2) Two-lamp ballasts
	2	F40T12/ES	1	MAG HC FO	Mag. Heater Cutout Full Light	66	
	3	F40T12/ES	1.5	MAG HC FO	Mag. Heater Cutout Full Light	99	Tandem wired
	4	F40T12/ES	2	MAG HC FO	Mag. Heater Cutout Full Light	132	(2) Two-lamp ballasts
	1	F40T12/ES	0.5	ELECT	Electronic	30	Tandem wired
	1	F40T12/ES	1	ELECT	Electronic	31	
	2	F40T12/ES	1	ELECT	Electronic	62	
	3	F40T12/ES	1	ELECT	Electronic	90	
	3	F40T12/ES	1.5	ELECT	Electronic	93	Tandem wired
	3	F40T12/ES	2	ELECT	Electronic	93	
	4	F40T12/ES	1	ELECT	Electronic	121	
	4	F40T12/ES	2	ELECT	Electronic	124	(2) Two-lamp ballasts

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
	2	F40T12/ES	1	ELECT AO	Elec. Adjustable Output (to 15%)	60	
	3	F40T12/ES	1.5	ELECT AO	Elec. Adjustable Output (to 15%)	90	Tandem wired
	4	F40T12/ES	2	ELECT AO	Elec. Adjustable Output (to 15%)	120	(2) Two-lamp ballasts
4 foot Fluorescent Rapid Start Stand. (40W)	1	F40T12	0.5	MAG.	Mag. Energy Efficient	44	Tandem wired
	1	F40T12	1	MAG.	Mag. Energy Efficient	46	
	2	F40T12	1	MAG.	Mag. Energy Efficient	88	
	3	F40T12	1	MAG.	Mag. Energy Efficient	127	
	3	F40T12	1.5	MAG.	Mag. Energy Efficient	132	Tandem wired
	3	F40T12	2	MAG.	Mag. Energy Efficient	134	
	4	F40T12	2	MAG.	Mag. Energy Efficient	176	(2) Two-lamp ballasts
	2	F40T12	1	MAG HC	Mag. Heater Cutout	71	
	3	F40T12	1.5	MAG HC	Mag. Heater Cutout	107	Tandem wired
	4	F40T12	2	MAG HC	Mag. Heater Cutout	142	(2) Two-lamp ballasts
4 foot Fluorescent Rapid Start Stand. (40W) <i>cont.</i>	2	°F40T12	1	MAG °F FO	Mag. Heater Cutout Full Light	80	
	3	°F40T12	1.5	MAG °F FO	Mag. Heater Cutout Full Light	120	Tandem wired
	4	°F40T12	2	MAG °F FO	Mag. Heater Cutout Full Light	160	(2) Two-lamp ballasts
	1	°F40T12	0.5	ELECT	Electronic	36	Tandem wired
	1	°F40T12	1	ELECT	Electronic	37	
	2	°F40T12	1	ELECT	Electronic	72	
	3	°F40T12	1	ELECT	Electronic	107	
	3	°F40T12	1.5	ELECT	Electronic	108	Tandem wired
	3	°F40T12	2	ELECT	Electronic	109	
	4	°F40T12	1	ELECT	Electronic	135	
	4	°F40T12	2	ELECT	Electronic	144	(2) Two-lamp ballasts
	2	°F40T12	1	ELECT RO	Electronic Reduce Output (75%)	61	
	3	°F40T12	1	ELECT RO	Electronic Reduce Output (75%)	90	

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
	3	°F40T12	1.5	ELECT RO	Electronic Reduce Output (75%)	92	Tandem wired
	4	°F40T12	2	ELECT RO	Electronic Reduce Output (75%)	122	(2) Two-lamp ballasts
	2	°F40T12	1	ELECT TL	Elec. Two Level (50 & 100%)	69	
	3	°F40T12	1.5	ELECT TL	Elec. Two Level (50 & 100%)	104	Tandem wired
	4	°F40T12	2	ELECT TL	Elec. Two Level (50 & 100%)	138	(2) Two-lamp ballasts
	2	°F40T12	1	ELECT AO	Elec. Adjustable Output (to 15%)	73	
	3	°F40T12	1.5	ELECT AO	Elec. Adjustable Output (to 15%)	110	Tandem wired
	4	°F40T12	2	ELECT AO	Elec. Adjustable Output (to 15%)	146	(2) Two-lamp ballasts
	2	°F40T12	1	ELECT DIM	Electronic Dimming (to 1%)	83	
	3	°F40T12	1.5	ELECT DIM	Electronic Dimming (to 1%)	125	Tandem wired
	4	°F40T12	2	ELECT DIM	Electronic Dimming (to 1%)	166	(2) Two-lamp ballasts

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-10 – Fluorescent Rapid Start High Output (HO) T8 &amp; T12, 8 ft

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
8 foot Fluorescent Rapid Start T8 High Output (86W)	1	F96T8/HO	1	ELECT	Electronic	88	
	2	F96T8/HO	1	ELECT	Electronic	160	
8 foot Fluorescent Rapid Start T12 High Output ("Energy-Saving" 95W)	1	F96T12/HO/ES	1	MAG STD	Mag. Stand.	125	
	2	F96T12/HO/ES	1	MAG STD**	Mag. Stand.	227	
	2	F96T12/HO/ES	1	MAG.	Mag. Energy Efficient	208	
	2	F96T12/HO/ES	1	ELECT	Electronic	170	
8 foot Fluorescent Rapid Start T12 High Output ("Stand." 110W)	1	F96T12/HO	1	MAG STD	Mag. Stand.	140	
	2	F96T12/HO	1	MAG STD**	Mag. Stand.	252	
	2	F96T12/HO	1	MAG.	Mag. Energy Efficient	237	
	1	F96T12/HO	1	ELECT	Electronic	119	
	2	F96T12/HO	1	ELECT	Electronic	205	
8 foot Fluorescent Rapid Start T12 Very High Output ("Energy-Saving" 195W)	1	F96T12/VHO/ES	1	MAG STD	Mag. Stand.	200	
	2	F96T12/VHO/ES	1	MAG STD	Mag. Stand.	325	
8 foot Fluorescent Rapid Start T12 Very High Output ("Stand." 215W)	1	Stand.96T12/VHO	1	MAG STAND.	Mag. Stand.	230	
	2	Stand.96T12/VHO	1	MAG STAND.	Mag. Stand.	440	

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-11 – Fluorescent Instant Start (single pin base "Slimline") T12, 4 ft

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
4 foot Fluorescent Slimline Energy-Saving T12 (32W)	1	Stand.48T12/ES	1	MAG STAND.	Mag. Stand.	51	
	2	Stand.48T12/ES	1	MAG STAND.	Mag. Stand.	82	
4 foot Fluorescent Slimline Stand. Stand. (39W)	1	Stand.48T12	1	MAG Stand.	Mag. Stand.	59	
	2	Stand.48T12	1	MAG Stand.	Mag. Stand.	98	

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-12 – Fluorescent Instant Start (single pin base "Slimline") T8 &amp; T12, 8 ft.

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
8 foot Fluorescent T8 Slimline (59W)	1	F96T8	1	MAG.	Mag. Stand.	58	
	2	F96T8	1	MAG.	Mag. Stand.	120	
	2	F96T8	1	ELECT NO	Electronic Normal Output	110	
	1	F96T8	1	ELECT HO	Electronic High Output	72	BF~1.10
	2	F96T8	1	ELECT HO1	Electronic High Output	140	BF~1.10
	2	F96T8	1	ELECT HO2	Electronic High Output	151	BF~1.20
8 foot Fluorescent T12 Slimline ("Energy-Saving" 60W)	1	F96T12/ES	1	MAG STD	Mag. Stand.	74	
	2	F96T12/ES	1	MAG STD**	Mag. Stand.	131	
	2	F96T12/ES	1	MAG.	Mag. Energy Efficient	112	
	1	F96T12/ES	1	ELECT	Electronic	70	
	2	F96T12/ES	1	ELECT	Electronic	107	
8 foot Fluorescent T12 Slimline ("Stand." 75W)	1	F96T12	1	MAG STD	Mag. Stand.	92	
	2	F96T12	1	MAG STD**	Mag. Stand.	158	
	2	F96T12	1	MAG.	Mag. Energy Efficient	144	
	1	F96T12	1	ELECT	Electronic	85	
	2	F96T12	1	ELECT	Electronic	132	
RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%							

Table NB-13 – High Intensity Discharge

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
Mercury Vapor	1	H40	1	MAG STD	Mag. Stand.	51	
	1	H50	1	MAG STD	Mag. Stand.	63	
	1	H75	1	MAG STD	Mag. Stand.	88	
	1	H100	1	MAG STD	Mag. Stand.	119	
	1	H175	1	MAG STD	Mag. Stand.	197	
	1	H250	1	MAG STD	Mag. Stand.	285	
	1	H400	1	MAG STD	Mag. Stand.	450	
	1	H1000	1	MAG STD	Mag. Stand.	1080	
Metal Halide	1	M35/39	1	MAG STD	Mag. Stand.	48	
	1	M35/39	1	ELECT	Electronic	44	
	1	M50	1	MAG STD	Mag. Stand.	68	
	1	M50	1	ELECT	Electronic	58	
	1	M70	1	MAG STD	Mag. Stand.	92	
	1	M70	1	ELECT	Electronic	86	
	1	M100	1	MAG STD	Mag. Stand.	122	
	1	M100	1	ELECT	Electronic	110	
	1	M125	1	MAG STD	Mag. Stand.	150	
	1	M150	1	MAG STD	Mag. Stand.	186	
	1	M150	1	ELECT	Electronic	168	
	1	M175	1	MAG STD	Mag. Stand.	205	
	1	M200	1	MAG STD	Mag. Stand.	232	
	1	M225	1	MAG STD	Mag. Stand.	258	
	1	M250	1	MAG STD	Mag. Stand.	295	
	1	M320	1	MAG STD	Mag. Stand.	365	
	1	M320	1	MAG LR	277v Linear Reactor	345	
	1	M360	1	MAG STD	Mag. Stand.	422	
	1	M360	1	MAG LR	277v Linear Reactor	388	
	1	M400	1	MAG STD	Mag. Stand.	461	
	1	M400	1	MAG LR	277v Linear Reactor	426	
	1	M450	1	MAG STD	Mag. Stand.	502	
	1	M450	1	MAG LR	277v Linear Reactor	478	
	1	M750	1	MAG STD	Mag. Stand.	820	
	1	M900	1	MAG STD	Mag. Stand.	990	
	1	M1000	1	MAG STD	Mag. Stand.	1080	
	1	M1500	1	MAG STD	Mag. Stand.	1650	
	1	M1650	1	MAG STD	Mag. Stand.	1810	

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
High Pressure Sodium	1	S35	1	MAG STD	Mag. Stand.	44	
	1	S50	1	MAG STD	Mag. Stand.	61	
	1	S70	1	MAG STD	Mag. Stand.	93	
	1	S100	1	MAG STD	Mag. Stand.	116	
	1	S150	1	MAG STD	Mag. Stand.	173	
	1	S200	1	MAG STD	Mag. Stand.	240	
	1	S250	1	MAG STD	Mag. Stand.	302	
	1	S400	1	MAG STD	Mag. Stand.	469	
High Pressure Sodium <i>cont.</i>	1	S1000	1	MAG STD	Mag. Stand.	1090	
Low Pressure Sodium	1	LPS18	1	MAG STAND.	Mag. Stand.	30	
	1	LPS35	1	MAG STAND.	Mag. Stand.	60	
	1	LPS55	1	MAG STAND.	Mag. Stand.	80	
	1	LPS90	1	MAG STAND.	Mag. Stand.	125	
	1	LPS135	1	MAG STAND.	Mag. Stand.	178	
	1	LPS180	1	MAG STAND.	Mag. Stand.	220	

RO = ballast factor 70 to 85%    NO = ballast factor 85 to 100%    HO = ballast factor >100%

Table NB-14 – 12 Volt Tungsten Halogen Lamps Including MR16, Bi-pin, AR70, AR111, PAR36

Type	Lamps		Ballasts			System Watts	Comment
	Number	Designation	Number	Designation	Description		
	1	20 watt lamp	1	ELECT	Electronic Power Supply	23	
	1	25 watt lamp	1	ELECT	Electronic Power Supply	28	
	1	35 watt lamp	1	ELECT	Electronic Power Supply	38	
	1	37 watt lamp	1	ELECT	Electronic Power Supply	41	
	1	42 watt lamp	1	ELECT	Electronic Power Supply	45	
	1	50 watt lamp	1	ELECT	Electronic Power Supply	54	
	1	65 watt lamp	1	ELECT	Electronic Power Supply	69	
	1	71 watt lamp	1	ELECT	Electronic Power Supply	75	
	1	75 watt lamp	1	ELECT	Electronic Power Supply	80	
	1	100 watt lamp	1	ELECT	Electronic Power Supply	106	
	1	20 watt lamp	1	MAG	Mag. Transformer	24	
	1	25 watt lamp	1	MAG	Mag. Transformer	29	
	1	35 watt lamp	1	MAG	Mag. Transformer	39	
	1	37 watt lamp	1	MAG	Mag. Transformer	42	
	1	42 watt lamp	1	MAG	Mag. Transformer	46	
	1	50 watt lamp	1	MAG	Mag. Transformer	55	
	1	65 watt lamp	1	MAG	Mag. Transformer	70	
	1	71 watt lamp	1	MAG	Mag. Transformer	76	
	1	75 watt lamp	1	MAG	Mag. Transformer	81	
	1	100 watt lamp	1	MAG	Mag. Transformer	108	



# NONRESIDENTIAL ACM MANUAL APPENDIX NC

## Appendix NC - Fan Motor Efficiencies

*Table NC-1 Fan Motor Efficiencies (< 1 HP)*

Nameplate or Brake Horsepower	Standard Fan Motor Efficiency	NEMA* High Efficiency	Premium Efficiency
1/20	40%	...	...
1/12	49%	...	...
1/8	55%	...	...
1/6	60%	...	...
1/4	64%	...	...
1/3	66%	...	...
1/2	70%	76.0%	80.0%
3/4	72%	77.0%	84.0%

*NOTE: For default drive efficiencies, see Table N2-17.*

\*NEMA - Proposed standard using test procedures.

Minimum NEMA efficiency per test IEEE 112b Rating Method.

Table NC-2 Fan Motor Efficiencies (1 HP and over)

Motor Horsepower	Open Motors				Enclosed Motors			
	2 pole 3600 rpm	4 pole 1800 rpm	6 pole 1200 rpm	8 pole 900 rpm	2 pole 3600 rpm	4 pole 1800 rpm	6 pole 1200 rpm	8 pole 900 rpm
1	—	82.5	80.0	74.0	75.5	82.5	80.0	74.0
1.5	82.5	84.0	84.0	75.5	82.5	84.0	85.5	77.0
2	84.0	84.0	85.5	85.5	84.0	84.0	86.5	82.5
3	84.0	86.5	86.5	86.5	85.5	87.5	87.5	84.0
5	85.5	87.5	87.5	87.5	87.5	87.5	87.5	85.5
7.5	87.5	88.5	88.5	88.5	88.5	89.5	89.5	85.5
10	88.5	89.5	90.2	89.5	89.5	89.5	89.5	88.5
15	89.5	91.0	92.0	89.5	90.2	91.0	90.2	88.5
20	90.2	91.0	91.0	90.2	90.2	91.0	90.2	89.5
25	91.0	91.7	91.7	90.2	91.0	92.4	91.7	89.5
30	91.0	92.4	92.4	91.0	91.0	92.4	91.7	91.0
40	91.7	93.0	93.0	91.0	91.7	93.0	93.0	91.0
50	92.4	93.0	93.0	91.7	92.4	93.0	93.0	91.7
60	93.0	93.6	93.6	92.4	93.0	93.6	93.6	91.7
75	93.0	94.1	93.6	93.6	93.0	94.1	93.6	93.0
100	93.0	94.1	94.1	93.6	93.6	94.5	94.1	93.0
125	93.6	94.5	94.1	93.6	94.5	94.5	94.1	93.6
150	93.6	95.0	94.5	93.6	94.5	95.0	95.0	93.6
200	94.5	95.0	94.5	93.6	95.0	95.0	95.0	94.1
250	94.5	95.0	95.4	94.5	95.4	95.0	95.0	94.5
300	95.0	95.4	95.4	—	95.4	95.4	95.0	—
350	95.0	95.4	95.4	—	95.4	95.4	95.0	—
400	95.4	95.4	—	—	95.4	95.4	—	—
450	95.8	95.8	—	—	95.4	95.4	—	—
500	95.8	95.8	—	—	95.4	95.8	—	—

## **NONRESIDENTIAL ACM MANUAL APPENDIX ND**

# **Appendix ND - Compliance Procedures for Relocatable Public School Buildings**

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### **ND.1 Purpose and Scope**

This document describes the compliance procedures that shall be followed when the whole building performance approach is used for relocatable public school buildings. Relocatable public school buildings are constructed (manufactured) at a central location and could be shipped and installed in any California climate zone. Furthermore, once they arrive at the school site, they could be positioned so that the windows face in any direction. The portable nature of relocatable classrooms requires that a special procedure be followed for showing compliance when the whole building performance method is used. Compliance documentation for relocatable public school buildings will be reviewed by the Division of the State Architect.

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### **ND.2 The Plan Check Process**

The Division of the State Architect (DSA) is the building department for relocatable public school buildings. Since relocatables are manufactured in batches, like cars or other manufactured products, the plan check and approval process occurs in two phases. The first phase is when the relocatable manufacturer completes design of a model or modifies a model. At this point, complete plans and specifications are submitted to the DSA; DSA reviews the plans for compliance with the energy standards and other California Building Code (CBC) requirements; and a "pre-check" (PC) design approval is granted. Once the PC design is approved, a school district or the manufacturer may file an "over-the-counter" application with DSA to construct one or more relocatables. The over-the-counter application is intended to be reviewed quickly, since the PC design has already been pre-checked. The over-the-counter application is the building permit application for construction and installation of a relocatable at a specific site, and includes the approved PC design drawings as well as site development plans for the proposed site where the relocatable will be installed. An over-the-counter application also is required for the construction of a stockpile of one or more relocatables based on the approved PC design drawings. Stockpiled relocatables are stored typically at the manufacturer's yard until the actual school site is determined where the relocatable will be installed. Another over-the-counter application is required to install a previously stockpiled relocatable at which time site development plans for the proposed site are checked.

The effective date for all buildings subject to the energy standards is the date of permit application. If a building permit application is submitted on or after the effective date, then the new energy standards apply. For relocatable classrooms, the date of the permit application is the date of the over-the-counter application, not the date of the application for PC design approval. The PC design is only valid until the code changes.

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### **ND.3 The Compliance Process**

Like other nonresidential buildings, the standard design for relocatable public school buildings is defined by the prescriptive requirements. In the case of relocatables, there are two choices of prescriptive criteria:

- Table 143-C in the Standards may be used for relocatable school buildings that can be installed in any climate zone in the state. In this case, the compliance is demonstrated in climates 14, 15, and 16 and this is accepted as evidence that the classroom will comply in all climate zones. These relocatables will have a permanent label that allows it to be used anywhere in the state.
- Table 143-A in the Standards may be used for relocatable school buildings that are to be installed in only specific climate zones. In this case, compliance is demonstrated in each climate zone for which the

relocatable has been designed to comply. These relocatables will have a permanent label that identifies in which climate zones it may be installed. It is not lawful to install the relocatable in other climate zones.

The building envelope of the standard design has the same geometry as the proposed design, including window area and position of windows on the exterior walls, and meets the prescriptive requirements specified in §143. Lighting power for the standard design meets the prescriptive requirements specified in §146. The HVAC system for the standard design meets the prescriptive requirements specified in §144. The system typically installed in relocatables is a single-zone packaged heat pump or furnace. Most relocatable school buildings do not have water heating systems, so this component is neutral in the analysis. Other modeling assumptions such as equipment loads, are the same for both the proposed design and the standard design and are specified in the Nonresidential ACM Manual.

Manufacturers shall certify compliance with the standards and all compliance documentation shall be provided. If the manufacturer chooses to comply using Table 143-A for compliance in only specific climate zones, then the manufacturers shall indicate the climate zones for which the classroom will be allowed to be located.

Since relocatable public school buildings could be positioned in any orientation, it is necessary to perform compliance calculations for multiple orientations. Each model with the same proposed design energy features shall be rotated through 12 different orientations either in climate zones 14, 15 and 16 for relocatables showing statewide compliance or in the specific climate zones that the manufacturer proposes for the relocatable to be allowed to be installed, i.e., the building with the same proposed design energy features is rotated in 30 degree increments and shall comply in each case. Approved compliance programs shall automate the rotation of the building and reporting of the compliance results to insure it is done correctly and uniformly and to avoid unnecessary documentation.

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#### **ND.4 Documentation**

The program shall present the results of the compliance calculations in a format similar to Table ND-1. For each of the cases (12 orientations times number of climates), the Time Dependent Valuation (TDV) energy for the *Standard Design* and the *Proposed Design* are shown (the energy features of the *Proposed Design* shall be the same for all orientations). The final column shows the compliance margin, which is the difference between the TDV energy for the *Proposed Design* and the *Standard Design*. Approved compliance programs shall scan the data presented in the Table ND-1 format and prominently highlight the case that has the smallest compliance margin. Complete compliance documentation shall be submitted for the building and energy features that achieve compliance in all of the climate zones and orientations as represented by the case with the smallest margin. DSA may require that compliance documentation for other cases also be submitted; showing that the *Proposed Design* building and energy features are identical to the case submitted, in each orientation and climate zone. Table ND-1 shows rows for climate zones 14, 15, and 16, which are the ones used when the criteria of Table 143-C is used to show compliance throughout the state. If the criteria of Table 143-A is used, then rows shall be added to the table for each climate zone for which the manufacturer wants the relocatable to be allowed to be installed.

Table ND-1 – Summary of Compliance Calculations Needed for Relocatable Classrooms

Climate Zone	Azimuth	TDV Energy		
		Proposed Design	Standard Design	Compliance Margin
14	0			
	30			
	60			
	90			
	120			
	150			
	180			
	210			
	240			
	270			
	300			
	330			
15	0			
	30			
	60			
	90			
	120			
	150			
	180			
	210			
	240			
	270			
	300			
	330			
16	0			
	30			
	60			
	90			
	120			
	150			
	180			
	210			
	240			
	270			
	300			
	330			

### ND.5 Optional Features

Relocatable classrooms may come with a variety of optional features, like cars. A school district can buy the “basic model” or it can pay for options. Many of the optional features do not affect energy efficiency and are not significant from the perspective of energy code compliance. Examples include floor finishes (various grades of carpet or tiles), casework, and ceiling and wall finishes. Other optional features do affect energy performance such as window construction, insulation, lighting systems, lighting controls, HVAC ductwork, HVAC equipment, and HVAC controls.

When a manufacturer offers a relocatable classroom model with a variety of options, it is necessary to identify those options that affect energy performance and to show that the model complies with any combination of the optional features. Most of the time, optional energy features are upgrades that clearly improve performance. If the basic model complies with the Standards, then adding any or all of the optional features would improve performance. The following are examples of optional features that are clear upgrades in terms of energy performance:

- HVAC equipment that has both a higher SEER and higher EER than the equipment in the basic model.
- Lighting systems that result in less power than the basic model.
- Lighting controls, such as occupancy sensors, that are recognized by the standards and for which power adjustment factors in Table 146-A are published in Section 146 of the Standards.
- Windows that have both a lower SHGC and lower U-factor (limited to relocatables that do not take credit for daylighting).
- Wall, roof or floor construction options that result in a lower U-factor than the basic model.

For energy code compliance purposes, it is necessary to show that every variation of the relocatable classroom that is offered to customers will comply with the Standards. There are two approaches for achieving this, as defined below:

**1) Basic Model Plus Energy Upgrades Approach** The simplest approach is to show that the basic model complies with the Standards and that all of the options that are offered to customers are clear energy upgrades that would only improve performance. As long as each and every measure in the basic model is met or exceeded by the energy upgrades, the relocatable classroom will comply with the standards.

While clear upgrades are obvious in most cases, the following are some examples of options that are not energy upgrades, for which additional analysis would be needed to show compliance that every combination of options comply.

- HVAC equipment that has a higher SEER, but a lower EER.
- Windows that lower SHGC but increase U-factor, or vice versa.
- Insulation options that reduce the U-factor for say walls, but increase it for the roof.
- Any other combination of measures that results in the performance of anyone measure being reduced in comparison to a complying basic model.

**2) Modeling of Every Combination Approach.** A more complex whole building performance approach is required when a model is available with options which in combination may or may not comply. In this case every combination of options shall be modeled, and the specific combinations that comply shall be determined and only those combinations shall be allowed. This approach, while possible, requires considerably more effort on the part of the relocatable manufacturer and its energy consultant. It also places a greater burden on DSA when they issue the over-the-counter building permit for the PC design that only allows specific combinations of energy options.. DSA would have to examine the specific optional features that are proposed with the over-the-counter application and make sure that the proposed combination of measures achieves compliance.

The manufacturer or its energy consultant would need to prepare a table or chart that shows all of the acceptable combinations that achieve compliance. This chart could be quite complex, depending on the number of optional features that are offered.

Table ND-2 is intended to illustrate the complexity that could be involved in modeling of every combination of energy features. It shows a list of typical optional features that would affect energy performance. In this example, there are two possible for each of the eight options, e.g the feature is either there or not (in an actual case there could be a different number of options and a different number of states for any option). In the example any one of the features could be combined with any of the others. The number of possible combinations in this example is two (the number of states) to the eighth power (the number of measures that

have two states). The number of possible options is then  $2^8$  or 256. This is the number of combinations that would need to be modeled in order to determine which combinations of optional features achieves compliance.

*Table ND-2 – Examples of Optional Features for Relocatable Classrooms*

Options Offered	States
1 Efficient lighting option	Yes/No
2 High efficiency heat pump	Yes/No
3 Improved wall insulation	Yes/No
4 Improved roof insulation	Yes/No
5 Occupancy sensor for lighting	Yes/No
6 Low -e windows	Yes/No
7 Skylights	Yes/No
8 Daylighting Controls	Yes/No

## **NONRESIDENTIAL ACM MANUAL APPENDIX NE**

### **Appendix NE**

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## **NONRESIDENTIAL ACM MANUAL APPENDIX NF**

### **Appendix NF - Technical Databases for Test Runs**

Table NF-1 – ACM MATERIAL LIBRARY
Table NF-2 – ACM LAYERS LIBRARY
Table NF-3 – ACM CONSTRUCTION LIBRARY
Table NF-4 – ACM VAV BOX LIBRARY
Table NF-5 – ACM PIU EQUIPMENT LIBRARY
Table NF-6 – ACM SMALL PACKAGE SPLIT AIR CONDITIONER
Table NF-7 – ACM LARGE PACKAGE SPLIT AIR CONDITIONER LIBRARY
Table NF-8 – ACM FAN COIL EQUIPMENT LIBRARY
Table NF-9 – ACM HEAT ONLY LIBRARY
Table NF-10 – ACM HEAT PUMP EQUIPMENT LIBRARY
Table NF-11 – ACM WATER LOOP EQUIPMENT LIBRARY
Table NF-12 – ACM EVAPORATIVE EQUIPMENT LIBRARY
Table NF-13 – ACM SYSTEM EQUIPMENT LIBRARY
Table NF-14 – ACM ELECTRICAL CHILLER LIBRARY
Table NF-15 – ACM ABSORPTION CHILLER LIBRARY
Table NF-16 – ACM TOWER LIBRARY
Table NF-17 – ACM BOILER LIBRARY
Table NF-18 – ACM VAV BOX SELECTED
Table NF-19 – ACM PACKAGE UNITS SELECTED
Table NF-20 – ACM WATER LOOP HEAT PUMP SELECTED
Table NF-21 – ACM EVAPORATIVE COOLING EQUIPMENT SELECTED
Table NF-22 – FAN COIL UNITS SELECTED
Table NF-23 – ACM HEAT PUMP EQUIPMENT SELECTED
Table NF-24 – ACM SYSTEM EQUIPMENT SELECTED
Table NF-25 – ACM CENTRAL COOLING EQUIPMENT SELECTED
Table NF-26 – ACM BOILER SELECTION

Table NF-1 – ACM MATERIAL LIBRARY

NAME	THICKNESS (feet)	CONDUCT.	DENSITY	SP-HEAT	R-VALUE
2X4	0.2917	0.0842	35.00	0.39	
2X6	0.4583	0.0842	35.00	0.39	
AIRWALL-MAT					1.00
CARPET2					2.00
CEL-2.5	0.2083	0.0333	5.00	0.32	
EARTH	1.0000	0.5000	85.00	0.20	
ISO-3.0	0.2500	0.0142	1.50	0.38	
PERIM	1.3330	0.9300	82.00	0.22	
R1.60					1.60
R1.95					1.95
R10-RIGID-INS	0.1667	0.0167	14.00	0.17	
R11-INS	0.2917	0.0265	0.60	0.20	
R13-INS	0.2917	0.0224	0.60	0.20	
R19-INS	0.5035	0.0265	0.60	0.20	
R30-INS	0.7500	0.0265	0.60	0.20	
R4-RIGID-INS	0.0833	0.0218	14.00	0.17	
R4.76					4.76
R5.93					5.93
R7-RIGID-INS	0.0833	0.0119	14.00	0.17	
SC2A	0.0729	0.4288	166.00	0.20	
SPANDREL-R10-MAT	1.0000	0.0100	25.00	0.20	
SPANDREL-R15-MAT	1.0000	0.0667	30.00	0.20	

Table NF-2 – ACM LAYERS LIBRARY

Name	Mat[1]	Mat[2]	Mat[3]	Mat[4]	Mat[5]	I-F-R
AIRWALL-LAY	AIRWALL-MAT					0.68
CONC-SPANDEL-LAY	CC22	W1B-R13	GP02			0.68
DEMISING-LAY	GP01	W1A-R11	GP01			0.68
DOORC-LAY	AS01	WD11	AS01			0.68
FLR-CONC-CAV-LAY	CEL-2.5	CC03	CP01			0.92
FLR-CONC-RAK-LAY	CEL-2.5	CC05	CP01			0.92
INTWALL-LAY	GP03	GP03	GP03			0.68
RF-INTERIOR-LAY	CC04	CP01				0.61
RF-ISO3.0-LAY	BR01	ISO-3.0	PW04			0.61
ROOFI-F-LAY	CC32	PW05	WD05	WD05		0.61
ROOFI-LAY	CC32	PW05				0.61
SLAB-LAY	EARTH	CC14				0.92
SLABC-LAY	EARTH	CC14	CP01			0.92
SLABP-LAY	EARTH	CC14	CP01			0.92
SPANDREL-R10-LAY	SPANDREL-R10-MAT					0.68
SPANDREL-R15-LAY	SPANDREL-R15-MAT					0.61
WIZ-LAY	GP02	W1A-R11	GP02			0.68

Table NF-3– ACM CONSTRUCTION LIBRARY

Construction	Layers	ABS	RO
AIRWALL	AIRWALL-LAY	0.7	3
CONC-SPANDEL	CONC-SPANDEL-LAY	0.7	3
DEMISING	DEMISING-LAY	0.7	3
DOORC	DOORC-LAY	0.7	3
FLR-CONC-CAV	FLR-CONC-CAV-LAY	0.7	3
FLR-CONC-RAK	FLR-CONC-RAK-LAY	0.7	3
INTWALL	INTWALL-LAY	0.7	3
RF-INTERIOR	RF-INTERIOR-LAY	0.7	3
RF-ISO3.0	RF-ISO3.0-LAY	0.7	3
ROOFI	ROOFI-LAY	0.7	3
ROOFI-F	ROOFI-F-LAY	0.7	3
SLAB	SLAB-LAY	0.1	3
SLABC	SLABC-LAY	0.1	3
SLABP	SLABP-LAY	0.1	3
SPANDREL-R10	SPANDREL-R10-LAY	0.7	3
SPANDREL-R15	SPANDREL-R15-LAY	0.4	3
WIZ	WIZ-LAY	0.7	3

Table NF-4 – ACM VAV BOX LIBRARY

MODEL	CFM	MIN RATIO	REHEAT CAP
VAV1200A	1200	0.35	21000
VAV1200H	1200	0.30	18000
VAV1200L	1200	0.40	24000
VAV1500A	1500	0.35	26250
VAV1500H	1500	0.30	22500
VAV1500L	1500	0.40	30000
VAV2000A	2000	0.35	35000
VAV2000H	2000	0.30	30000
VAV2000L	2000	0.40	40000
VAV2500A	2500	0.35	43750
VAV2500H	2500	0.30	37500
VAV2500L	2500	0.40	50000
VAV3000A	3000	0.35	52500
VAV3000H	3000	0.30	45000
VAV3000L	3000	0.40	60000
VAV300A	300	0.35	5250
VAV300H	300	0.30	4500
VAV300L	300	0.40	6000
VAV3500A	3500	0.35	61250
VAV3500H	3500	0.30	52500
VAV3500L	3500	0.40	70000
VAV4000A	4000	0.35	70000
VAV4000H	4000	0.30	60000
VAV4000L	4000	0.40	80000
VAV4500A	4500	0.35	78750
VAV4500H	4500	0.30	67500
VAV4500L	4500	0.40	90000
VAV450A	450	0.35	7875
VAV450H	450	0.30	6750
VAV450L	450	0.40	9000
VAV5000A	5000	0.35	87500
VAV5000H	5000	0.30	75000
VAV5000L	5000	0.40	100000
VAV600A	600	0.35	10500
VAV600H	600	0.30	9000
VAV600L	600	0.40	12000
VAV900A	900	0.35	15750

MODEL	CFM	MIN RATIO	REHEAT CAP
VAV900H	900	0.30	13500
VAV900L	900	0.40	18000

Table NF-5 – ACM PIU EQUIPMENT LIBRARY

Model	TYP	Cfm	M-C-R	F-C-R	FPI	ReheatCap
PIU300AP	P	300	0.3	0.60	0.33	8100
PIU300AS	S	300	0.3	1.00	0.33	8100
PIU300HP	P	300	0.3	0.90	0.28	12000
PIU300HS	S	300	0.3	1.00	0.28	12000
PIU300LP	P	300	0.3	0.40	0.35	5400
PIU300LS	S	300	0.3	1.00	0.35	5400
PIU450AP	P	450	0.3	0.60	0.33	12000
PIU450AS	S	450	0.3	1.00	0.33	12000
PIU450HP	P	450	0.3	0.90	0.28	18200
PIU450HS	S	450	0.3	1.00	0.28	18200
PIU450LP	P	450	0.3	0.40	0.35	8100
PIU450LS	S	450	0.3	1.00	0.35	8100
PIU600AP	P	600	0.3	0.60	0.33	16200
PIU600AS	S	600	0.3	1.00	0.33	16200
PIU600HP	P	600	0.3	0.90	0.28	24300
PIU600HS	S	600	0.3	1.00	0.28	24300
PIU600LP	P	600	0.3	0.40	0.35	10800
PIU600LS	S	600	0.3	1.00	0.35	10800
PIU750AP	P	750	0.3	0.60	0.33	20250
PIU750AS	S	750	0.3	1.00	0.33	20250
PIU750HP	P	750	0.3	0.90	0.28	30400
PIU750HS	S	750	0.3	1.00	0.28	20250
PIU750LP	P	750	0.3	0.40	0.35	13500
PIU750LS	S	750	0.3	1.00	0.35	13500
PIU900AP	P	900	0.3	0.60	0.33	24300
PIU900AS	S	900	0.3	1.00	0.33	24300
PIU900HP	P	900	0.3	0.90	0.28	36500
PIU900HS	S	900	0.3	1.00	0.28	36500
PIU900LP	P	900	0.3	0.40	0.35	16200
PIU900LS	S	900	0.3	1.00	0.35	16200

Table NF-6— ACM SMALL PACKAGE SPLIT AIR CONDITIONER

Model	Cap95	Cap82	EER	SEER	CFM	Cd	FPIcv	FPIvav	HCAP	AFUE
ACSP17A	17000	18850	9.60	9.90	500	0.15	0.50	1.00	25000	82
ACSP17H	17000	17860	9.70	10.00	500	0.20	0.35	0.75	25000	84
ACSP17L	17000	20200	9.50	9.90	500	0.10	0.90	1.30	25000	80
ACSP22A	22000	24270	9.60	9.90	600	0.15	0.50	1.00	30000	82
ACSP22H	22000	24700	10.40	12.00	600	0.20	0.35	0.75	30000	84
ACSP22L	22000	24640	9.50	9.90	600	0.10	0.90	1.30	30000	82
ACSP28A	28000	31310	9.60	9.90	800	0.15	0.50	1.00	40000	84
ACSP28H	28000	31320	10.60	12.00	800	0.20	0.35	0.75	40000	80
ACSP28L	28000	31420	9.50	9.90	800	0.10	0.90	1.30	40000	82
ACSP34A	34000	36850	9.60	9.90	1100	0.15	0.50	1.00	55000	84
ACSP34H	34000	37770	10.50	12.00	1100	0.20	0.35	0.75	55000	80
ACSP34L	34000	38370	9.50	9.90	1100	0.10	0.90	1.30	55000	82
ACSP40A	40000	43360	9.60	9.90	1200	0.15	0.50	1.00	60000	84
ACSP40H	40000	42530	10.80	12.00	1200	0.20	0.35	0.75	60000	80
ACSP40L	40000	46820	9.50	9.90	1200	0.10	0.90	1.30	60000	82
ACSP46A	46000	49770	9.60	9.90	1600	0.15	0.50	1.00	80000	84
ACSP46H	46000	51400	10.50	12.00	1600	0.20	0.35	0.75	80000	80
ACSP46L	46000	49660	9.50	9.90	1600	0.10	0.90	1.30	80000	82
ACSP52A	52000	55500	9.60	9.90	1700	0.15	0.50	1.00	85000	84
ACSP52H	52000	56280	11.10	12.50	1700	0.20	0.35	0.75	85000	80
ACSP52L	52000	56650	9.50	9.90	1700	0.10	0.90	1.30	85000	82
ACSP58A	58000	62520	9.60	9.90	1800	0.15	0.50	1.00	90000	84
ACSP58H	58000	62290	10.80	12.00	1800	0.20	0.35	0.75	90000	80
ACSP58L	58000	63360	9.50	9.90	1800	0.10	0.90	1.30	90000	82
ACSP63A	63000	67460	9.60	9.90	1900	0.15	0.50	1.00	95000	84
ACSP63H	63000	68000	10.50	12.10	1900	0.20	0.35	0.75	95000	80
ACSP63L	63000	67830	9.50	9.90	1900	0.10	0.90	1.30	95000	82

Table NF-7– ACM LARGE PACKAGE SPLIT AIR CONDITIONER LIBRARY

Model	Cap95	Cfm	BHPari	MotorEff	FPLcv	FPLvav	EER	HCap	AFUE
ACLP007A	80150	3100	0.23	0.810	0.50	1.00	9.00	93000	82
ACLP007H	79100	2800	0.21	0.875	0.35	0.75	9.20	84000	84
ACLP007L	77350	2500	0.18	0.810	0.90	1.30	8.90	75000	80
ACLP010A	114500	4500	0.41	0.850	0.50	1.00	9.00	135000	82
ACLP010H	113000	4000	0.34	0.917	0.35	0.75	9.20	120000	84
ACLP010L	110500	3500	0.30	0.850	0.90	1.30	8.90	105000	80
ACLP015A	171750	6750	0.85	0.850	0.50	1.00	8.70	202500	82
ACLP015H	169500	6000	0.67	0.917	0.35	0.75	9.00	180000	84
ACLP015L	165750	5250	0.38	0.850	0.90	1.30	8.50	157500	80
ACLP020A	229000	9000	1.60	0.850	0.50	1.00	8.70	270000	82
ACLP020H	226000	8000	1.23	0.917	0.35	0.75	9.00	240000	84
ACLP020L	221000	7000	0.92	0.850	0.90	1.30	8.50	210000	80
ACLP025A	292000	8750	1.34	0.850	0.50	1.00	8.70	262500	82
ACLP025H	281000	7000	0.79	0.917	0.35	0.75	9.00	210000	84
ACLP025L	271500	6000	0.50	0.850	0.90	1.30	8.50	180000	80
ACLP030A	352000	12000	2.13	0.850	0.50	1.00	8.70	360000	82
ACLP030H	345000	10500	1.40	0.917	0.35	0.75	9.00	315000	84
ACLP030L	337000	9000	1.09	0.850	0.90	1.30	8.50	270000	80
ACLP040A	483000	18000	4.13	0.860	0.50	0.75	8.70	540000	82
ACLP040H	476000	16000	3.02	0.910	0.35	0.75	9.00	480000	84
ACLP040L	467000	14000	2.12	0.860	0.90	1.30	8.50	420000	80
ACLP050A	589000	22500	7.60	0.860	0.50	1.00	8.70	675000	82
ACLP050H	580000	20000	5.49	0.910	0.35	0.75	9.00	600000	84
ACLP050L	569000	17500	3.75	0.860	0.90	1.30	8.50	525000	80
ACLP060A	723000	27000	7.26	0.880	0.50	1.00	8.70	810000	82
ACLP060H	712000	24000	5.41	0.930	0.35	0.75	9.00	720000	84
ACLP060L	698000	21000	3.91	0.880	0.90	1.30	8.50	630000	80
ACLP070A	811000	26000	6.60	0.880	0.50	1.00	8.50	780000	82
ACLP070H	801000	24000	5.41	0.930	0.35	0.75	8.80	720000	84
ACLP070L	815000	27000	7.26	0.880	0.90	1.30	8.20	810000	80
ACLP075A	883000	26000	6.60	0.880	0.50	1.00	8.50	780000	82
ACLP075H	873000	24000	5.41	0.930	0.35	0.75	8.80	720000	84
ACLP075L	862000	22000	3.91	0.880	0.90	1.30	8.20	660000	80
ACLP090A	1062000	42000	15.03	0.880	0.50	1.00	8.70	1260000	82
ACLP090H	1044000	37000	10.82	0.930	0.35	0.75	8.80	1110000	84
ACLP090L	1021000	32000	7.52	0.880	0.90	1.30	8.20	960000	80
ACLP105A	1229000	43000	15.99	0.890	0.50	1.00	8.50	1290000	82
ACLP105H	1213000	39000	12.39	0.941	0.35	0.75	8.80	1170000	84

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Model	Cap95	Cfm	BHPari	MotorEff	FPlcv	FPlvav	EER	HCap	AFUE
ACLP105L	1193000	35000	9.40	0.880	0.90	1.30	8.20	1050000	80

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Table NF-8– ACM FAN COIL EQUIPMENT LIBRARY

MODEL	COOLCAP	HEATCAP	CFM	FPI
FC008A	8400	12000	300	0.50
FC008H	8400	12000	300	0.35
FC008L	8400	12000	300	0.90
FC013A	12600	18000	450	0.50
FC013H	12600	18000	450	0.35
FC013L	12600	18000	450	0.90
FC017A	16800	24000	600	0.50
FC017H	16800	24000	600	0.35
FC017L	16800	24000	600	0.90
FC021A	21000	30000	750	0.50
FC021H	21000	30000	750	0.35
FC021L	21000	30000	750	0.90
FC028A	28000	40000	1000	0.50
FC028H	28000	40000	1000	0.35
FC028L	28000	40000	1000	0.90
FC035A	35000	50000	1250	0.50
FC035H	35000	50000	1250	0.35
FC035L	35000	50000	1250	0.90
FC042A	42000	60000	1500	0.50
FC042H	42000	60000	1500	0.35
FC042L	42000	60000	1500	0.90
FC056A	56000	80000	2000	0.50
FC056H	56000	80000	2000	0.35
FC056L	56000	80000	2000	0.90
FC070A	70000	100000	2500	0.50
FC070H	70000	100000	2500	0.35
FC070L	70000	100000	2500	0.90
FC084A	84000	120000	3000	0.50
FC084H	84000	120000	3000	0.35
FC084L	84000	120000	3000	0.90
FC098A	98000	140000	3500	0.50
FC098H	98000	140000	3500	0.35
FC098L	98000	140000	3500	0.90
FC112A	112000	160000	4000	0.50
FC112H	112000	160000	4000	0.35
FC112L	112000	160000	4000	0.90
FC126A	126000	180000	4500	0.50
FC126H	126000	180000	4500	0.35
FC126L	126000	180000	4500	0.90

MODEL	COOLCAP	HEATCAP	CFM	FPI
FC140A	140000	200000	5000	0.50
FC140H	140000	200000	5000	0.35
FC140L	140000	200000	5000	0.90
FC168A	168000	240000	6000	0.50
FC168H	168000	240000	6000	0.35
FC168L	168000	240000	6000	0.90
FC196A	196000	280000	7000	0.50
FC196H	196000	280000	7000	0.35
FC196L	196000	280000	7000	0.90
FC224A	224000	320000	8000	0.50
FC224H	224000	320000	8000	0.35
FC224L	224000	320000	8000	0.90
FC252A	252000	360000	9000	0.50
FC252H	252000	360000	9000	0.35
FC252L	252000	360000	9000	0.90
FC280A	280000	400000	10000	0.50
FC280H	280000	400000	10000	0.35
FC280L	280000	400000	10000	0.90
FC350A	350000	500000	12500	0.50
FC350H	350000	500000	12500	0.35
FC350L	350000	500000	12500	0.90
FC420A	420000	600000	15000	0.50
FC420H	420000	600000	15000	0.35
FC420L	420000	600000	15000	0.90
FC490A	490000	700000	17500	0.50
FC490H	490000	700000	17500	0.35
FC490L	490000	700000	17500	0.90
FC560A	560000	800000	20000	0.50
FC560H	560000	800000	20000	0.35
FC560L	560000	800000	20000	0.90
FC700A	700000	1000000	25000	0.50
FC700H	700000	1000000	25000	0.35
FC700L	700000	1000000	25000	0.90
FC840A	840000	1200000	30000	0.50
FC840H	840000	1200000	30000	0.35
FC840L	840000	1200000	30000	0.90

Table NF-9— ACM HEAT ONLY LIBRARY

Model	HeatCap	CFM	FPI	AFUE
HEAT045A	45000	1000	0.50	82
HEAT045H	45000	1000	0.35	84
HEAT045L	45000	1000	0.90	80
HEAT063A	63000	1500	0.50	82
HEAT063H	63000	1500	0.35	84
HEAT063L	63000	1500	0.90	80
HEAT090A	90000	2000	0.50	82
HEAT090H	90000	2000	0.35	84
HEAT090L	90000	2000	0.90	80
HEAT108A	108000	2500	0.50	82
HEAT108H	108000	2500	0.35	84
HEAT108L	108000	2500	0.90	80
HEAT135A	135000	3000	0.50	82
HEAT135H	135000	3000	0.35	84
HEAT135L	135000	3000	0.90	80
HEAT153A	153000	3500	0.50	82
HEAT153H	153000	3500	0.35	84
HEAT153L	153000	3500	0.90	80
HEAT180A	180000	4000	0.50	82
HEAT180H	180000	4000	0.35	84
HEAT180L	180000	4000	0.90	80
HEAT215A	215000	5000	0.50	82
HEAT215H	215000	5000	0.35	84
HEAT215L	215000	5000	0.90	80
HEAT323A	323000	7500	0.50	82
HEAT323H	323000	7500	0.35	84
HEAT323L	323000	7500	0.90	80
HEAT450A	450000	10000	0.50	82
HEAT450H	450000	10000	0.35	84
HEAT450L	450000	10000	0.90	80
HEAT538A	538000	12500	0.50	82
HEAT538H	538000	12500	0.35	84
HEAT538L	538000	12500	0.90	80
HEAT665A	665000	15000	0.50	82
HEAT665H	665000	15000	0.35	84
HEAT665L	665000	15000	0.90	80
HEAT900A	900000	20000	0.50	82
HEAT900H	900000	20000	0.35	84

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Model	HeatCap	CFM	FPI	AFUE
HEAT900L	900000	20000	0.90	80

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Table NF-10– ACM HEAT PUMP EQUIPMENT LIBRARY

Model	Cap 95	Cap 82	Hcap 47	Hcap 17	EER	SEER	HSPF	COP 47	COP 17	Cfm	Cd	Fpi
HPSP108A	108000		110000	58700	9.00		7.32	3.00	2.00	3300		0.50
HPSP108H	108000		109800	56300	9.20		7.32	3.00	2.00	3300		0.35
HPSP108L	108000		109800	59000	8.90		7.68	3.10	2.00	3300		0.90
HPSP126A	126000		123400	68100	9.00		7.32	3.00	2.00	4300		0.50
HPSP126H	126000		111700	59900	9.60		7.32	3.00	2.00	4300		0.35
HPSP126L	126000		128100	68900	8.90		7.68	3.10	2.00	4300		0.90
HPSP162A	162000		150600	80200	8.90		7.00	2.90	2.00	5400		0.50
HPSP162H	162000		146400	77600	9.40		7.00	2.90	2.00	5400		0.35
HPSP162L	162000		148800	77200	8.50		7.00	2.90	2.00	5400		0.90
HPSP222A	222000		224200	115400	8.60		7.32	3.00	2.00	6400		0.50
HPSP222H	222000		215900	115000	8.80		7.32	3.00	2.00	6400		0.35
HPSP222L	222000		227700	123500	8.50		7.32	3.00	2.10	6400		0.90
HPSP22A	22000	24150	21600	11900	9.60	10.50	7.32	3.00	2.00	600	0.15	0.50
HPSP22H	22000	24050	20800	10900	11.10	12.00	8.40	3.30	2.00	600	0.20	0.35
HPSP22L	22000	23390	22000	12300	9.50	10.00	7.32	3.00	2.00	600	0.10	0.90
HPSP28A	28000	30420	27500	15400	9.60	10.40	7.32	3.00	2.00	800	0.15	0.50
HPSP28H	28000	30040	25400	13900	11.20	12.00	7.32	3.00	2.00	800	0.20	0.35
HPSP28L	28000	30800	28000	15800	9.50	9.90	7.32	3.00	2.00	800	0.10	0.90
HPSP34A	34000	36980	33500	18600	9.60	10.20	7.32	3.00	2.00	1100	0.15	0.50
HPSP34H	34000	37600	31100	18000	10.70	12.00	8.40	3.30	2.20	1100	0.20	0.35
HPSP34L	34000	37790	36300	19600	9.50	9.90	7.32	3.00	2.00	1100	0.10	0.90
HPSP40A	40000	43500	39600	22000	9.60	10.00	7.32	3.00	2.00	1200	0.15	0.50
HPSP40H	40000	44140	37200	20700	10.30	12.00	8.04	3.20	2.00	1200	0.20	0.35
HPSP40L	40000	44930	41400	24000	9.50	9.90	7.32	3.00	2.00	1200	0.10	0.90
HPSP46A	46000	50000	46200	25700	9.60	10.00	7.32	3.00	2.00	1600	0.15	0.50
HPSP46H	46000	51400	46500	25600	10.40	12.00	8.04	3.20	2.10	1600	0.20	0.35
HPSP46L	46000	49830	48100	26200	9.50	9.90	7.68	3.10	2.10	1600	0.10	0.90
HPSP52A	52000	56060	51300	28000	9.60	10.00	7.32	3.00	2.00	1700	0.15	0.50
HPSP52H	52000	56820	49300	28900	9.90	12.30	8.04	3.20	2.00	1700	0.20	0.35
HPSP52L	52000	56280	51400	30000	9.50	9.90	7.32	3.00	2.00	1700	0.10	0.90
HPSP58A	58000	62530	59000	33800	9.60	10.00	7.68	3.10	2.10	1800	0.15	0.50
HPSP58H	58000	64710	58000	31500	10.10	12.00	8.40	3.30	2.20	1800	0.20	0.35
HPSP58L	58000	62140	60000	33900	9.50	9.90	7.32	3.00	2.10	1800	0.10	0.90
HPSP63A	63000	66900	60800	34300	9.60	10.00	7.32	3.00	2.00	1900	0.15	0.50
HPSP63H	63000	67260	58900	32100	9.70	10.50	7.32	3.00	2.00	1900	0.20	0.35
HPSP63L	63000	67190	59400	32600	9.50	9.90	7.32	3.00	2.00	1900	0.10	0.90
HPSP72A	72000		70600	38200	9.00		7.32	3.00	2.00	2400		0.50
HPSP72H	72000		71600	44400	9.50		7.68	3.10	2.00	2400		0.35

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Model	Cap 95	Cap 82	Hcap 47	Hcap 17	EER	SEER	HSPF	COP 47	COP 17	Cfm	Cd	Fpi
HPSP72L	72000		72000	35400	8.90		7.32	3.00	2.00	2400		0.90
HPSP90A	90000		90500	49300	9.00		7.32	3.00	2.00	2600		0.50
HPSP90H	90000		83400	54100	9.40		7.32	3.00	2.10	2600		0.35
HPSP90L	90000		88900	44400	8.90		7.32	3.00	2.00	2600		0.90

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Table NF-11– ACM WATER LOOP EQUIPMENT LIBRARY

MODEL	COOLCAP	EER	HEATCAP	COP	CFM	FPI
WHP007A	7000	11.50	8050	4.00	230	0.50
WHP007H	7000	15.00	8050	4.50	230	0.35
WHP007L	7000	10.00	8050	3.80	230	0.85
WHP009A	9000	11.50	10350	4.00	300	0.50
WHP009H	9000	15.00	10350	4.50	300	0.35
WHP009L	9000	10.00	10350	3.80	300	0.85
WHP012A	12000	11.50	13800	4.00	400	0.50
WHP012H	12000	15.00	13800	4.50	400	0.35
WHP012L	12000	10.00	13800	3.80	400	0.85
WHP015A	15000	11.50	17250	4.00	500	0.50
WHP015H	15000	15.00	17250	4.50	500	0.35
WHP015L	15000	10.00	17250	3.80	500	0.85
WHP018A	18000	11.50	20700	4.00	600	0.50
WHP018H	18000	15.00	20700	4.50	600	0.35
WHP018L	18000	10.00	20700	3.80	600	0.85
WHP024A	24000	11.50	27600	4.00	800	0.50
WHP024H	24000	15.00	27600	4.50	800	0.35
WHP024L	24000	10.00	27600	3.80	800	0.85
WHP030A	30000	11.50	34500	4.00	1000	0.50
WHP030H	30000	15.00	34500	4.50	1000	0.35
WHP030L	30000	10.00	34500	3.80	1000	0.85
WHP036A	36000	11.50	41400	4.00	1200	0.50
WHP036H	36000	15.00	41400	4.50	1200	0.35
WHP036L	36000	10.00	41400	3.80	1200	0.85
WHP042A	42000	11.50	48300	4.00	1400	0.50
WHP042H	42000	15.00	48300	4.50	1400	0.35
WHP042L	42000	10.00	48300	3.80	1400	0.85
WHP048A	48000	11.50	55200	4.00	1600	0.50
WHP048H	48000	15.00	55200	4.50	1600	0.35
WHP048L	48000	10.00	55200	3.80	1600	0.85
WHP060A	60000	11.50	69000	4.00	2000	0.50
WHP060H	60000	15.00	69000	4.50	2000	0.35
WHP060L	60000	10.00	69000	3.80	2000	0.85
WHP072A	72000	11.50	82800	4.00	2400	0.50
WHP072H	72000	15.00	82800	4.50	2400	0.35
WHP072L	72000	10.50	82800	3.80	2400	0.85
WHP084A	84000	11.50	96600	4.00	2800	0.50
WHP084H	84000	15.00	96600	4.50	2800	0.35

MODEL	COOLCAP	EER	HEATCAP	COP	CFM	FPI
WHP084L	84000	10.50	96600	3.80	2800	0.85
WHP096A	96000	11.50	110400	4.00	3200	0.50
WHP096H	96000	15.00	110400	4.50	3200	0.35
WHP096L	96000	10.50	110400	3.80	3200	0.85
WHP108A	108000	11.50	124200	4.00	3600	0.50
WHP108H	108000	15.00	124200	4.50	3600	0.35
WHP108L	108000	10.50	124200	3.80	3600	0.85
WHP120A	120000	11.50	138000	4.00	4000	0.50
WHP120H	120000	15.00	138000	4.50	4000	0.35
WHP120L	120000	10.50	138000	3.80	4000	0.85
WHP132A	132000	11.50	151800	4.00	4400	0.50
WHP132H	132000	15.00	151800	4.50	4400	0.35
WHP132L	132000	10.50	151800	3.80	4400	0.85

Table NF-12– ACM EVAPORATIVE EQUIPMENT LIBRARY

Model	Cfm	IndirEff	DirEff	FPI	FPIsup	ACbackUp
EVAP1000AIB	1000	85		0.696	0.500	ACSP58A
EVAP1000AID	1000	85	78	0.696	0.500	
EVAP1000HIB	1000	85		0.546	0.240	ACSP58H
EVAP1000HID	1000	85	78	0.546	0.240	
EVAP1000LIB	1000	85		0.996	0.600	ACSP58L
EVAP1000LID	1000	85	78	0.996	0.600	
EVAP1300AIB	1300	85		0.696	0.500	ACSP63A
EVAP1300AID	1300	85	78	0.696	0.500	
EVAP1300HIB	1300	85		0.546	0.240	ACSP63H
EVAP1300HID	1300	85	78	0.546	0.240	
EVAP1300LIB	1300	85		0.996	0.600	ACSP63L
EVAP1300LID	1300	85	78	0.996	0.600	
EVAP1500AIB	1500	85		0.696	0.500	ACLP007A
EVAP1500AID	1500	85	78	0.696	0.500	
EVAP1500HIB	1500	85		0.546	0.240	ACLP007H
EVAP1500HID	1500	85	78	0.546	0.240	
EVAP1500LIB	1500	85		0.996	0.600	ACLP007L
EVAP1500LID	1500	85	78	0.996	0.600	
EVAP2000AIB	2000	85		0.696	0.500	ACLP007A
EVAP2000AID	2000	85	78	0.696	0.500	
EVAP2000HIB	2000	85		0.546	0.240	ACLP007H
EVAP2000HID	2000	85	78	0.546	0.240	
EVAP2000LIB	2000	85		0.996	0.600	ACLP007L



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Model	Cfm	IndirEff	DirEff	FPI	FPIsup	ACbackUp
EVAP2000LID	2000	85	78	0.996	0.600	
EVAP2500AIB	2500	85		0.696	0.500	ACLP007A
EVAP2500AID	2500	85	78	0.696	0.500	
EVAP2500HIB	2500	85		0.546	0.240	ACLP007H
EVAP2500HID	2500	85	78	0.546	0.240	
EVAP2500LIB	2500	85		0.996	0.600	ACLP007L
EVAP2500LID	2500	85	78	0.996	0.600	

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Table NF-13– ACM SYSTEM EQUIPMENT LIBRARY

MODEL	COOLCAP	HEATCAP	CFM	FPIcv	FPIvav
SYS0025A	25000	33929	893	0.50	1.00
SYS0025H	25000	33929	893	0.35	0.75
SYS0025L	25000	33929	893	0.90	1.35
SYS0038A	38000	51571	1357	0.50	1.00
SYS0038H	38000	51571	1357	0.35	0.75
SYS0038L	38000	51571	1357	0.90	1.35
SYS0050A	50000	67857	1786	0.50	1.00
SYS0050H	50000	67857	1786	0.35	0.75
SYS0050L	50000	67857	1786	0.90	1.35
SYS0063A	63000	85500	2250	0.50	1.00
SYS0063H	63000	85500	2250	0.35	0.75
SYS0063L	63000	85500	2250	0.90	1.35
SYS0075A	75000	101786	2679	0.50	1.00
SYS0075H	75000	101786	2679	0.35	0.75
SYS0075L	75000	101786	2679	0.90	1.35
SYS0088A	88000	119429	3143	0.50	1.00
SYS0088H	88000	119429	3143	0.35	0.75
SYS0088L	88000	119429	3143	0.90	1.35
SYS0100A	100000	135714	3571	0.50	1.00
SYS0100H	100000	135714	3571	0.35	0.75
SYS0100L	100000	135714	3571	0.90	1.35
SYS0125A	125000	169643	4464	0.50	1.00
SYS0125H	125000	169643	4464	0.35	0.75
SYS0125L	125000	169643	4464	0.90	1.35
SYS0188A	188000	255143	6714	0.50	1.00
SYS0188H	188000	255143	6714	0.35	0.75
SYS0188L	188000	255143	6714	0.90	1.35
SYS0250A	250000	339286	8929	0.50	1.00
SYS0250H	250000	339286	8929	0.35	0.75
SYS0250L	250000	339286	8929	0.90	1.35
SYS0380A	380000	515714	13571	0.50	1.00
SYS0380H	380000	515714	13571	0.35	0.75
SYS0380L	380000	515714	13571	0.90	1.35
SYS0500A	500000	678571	17857	0.50	1.00
SYS0500H	500000	678571	17857	0.35	0.75
SYS0500L	500000	678571	17857	0.90	1.35
SYS0625A	625000	848214	22321	0.50	1.00
SYS0625H	625000	848214	22321	0.35	0.75

MODEL	COOLCAP	HEATCAP	CFM	FPIcv	FPIvav
SYS0625L	625000	848214	22321	0.90	1.35
SYS0750A	750000	1017857	26786	0.50	1.00
SYS0750H	750000	1017857	26786	0.35	0.75
SYS0750L	750000	1017857	26786	0.90	1.35
SYS1000A	1000000	1357143	33000	0.50	1.00
SYS1000H	1000000	1357143	33000	0.35	0.75
SYS1000L	1000000	1357143	33000	0.90	1.35

Table NF-14– ACM ELECTRICAL CHILLER LIBRARY

Model	CoolCap	COP
COOL0180A	180000	4.00
COOL0180H	180000	4.20
COOL0180L	180000	3.80
COOL0240A	240000	4.00
COOL0240H	240000	4.20
COOL0240L	240000	3.80
COOL0300A	300000	4.00
COOL0300H	300000	4.20
COOL0300L	300000	3.80
COOL0360A	360000	4.00
COOL0360H	360000	4.20
COOL0360L	360000	3.80
COOL0480A	480000	4.00
COOL0480H	480000	4.20
COOL0480L	480000	3.80
COOL0900A	900000	4.00
COOL0900H	900000	4.20
COOL0900L	900000	3.80
COOL1200A	1200000	4.00
COOL1200H	1200000	4.20
COOL1200L	1200000	3.80
COOL1800A	1800000	4.40
COOL1800H	1800000	4.60
COOL1800L	1800000	4.20
COOL2100A	2100000	4.40
COOL2100H	2100000	4.60
COOL2100L	2100000	4.20
COOL2400A	2400000	4.40
COOL2400H	2400000	4.60

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Model	CoolCap	COP
COOL2400L	2400000	4.20
COOL3000A	3000000	4.40
COOL3000H	3000000	4.60
COOL3000L	3000000	4.20
COOL3600A	3600000	5.60
COOL3600H	3600000	5.80
COOL3600L	3600000	5.20
COOL4200A	4200000	5.60
COOL4200H	4200000	5.80
COOL4200L	4200000	5.20

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Table NF-15– ACM ABSORPTION CHILLER LIBRARY

Model	Cooling Capacity	HIR	EIR
ABSOR10180A	180000	1.60	0.0040
ABSOR10180H	180000	1.55	0.0035
ABSOR10180L	180000	1.65	0.0045
ABSOR10240A	240000	1.60	0.0040
ABSOR10240H	240000	1.55	0.0035
ABSOR10240L	240000	1.65	0.0045
ABSOR10300A	300000	1.60	0.0040
ABSOR10300H	300000	1.55	0.0035
ABSOR10300L	300000	1.65	0.0045
ABSOR10360A	360000	1.60	0.0040
ABSOR10360H	360000	1.55	0.0035
ABSOR10360L	360000	1.65	0.0045
ABSOR10480A	480000	1.60	0.0040
ABSOR10480H	480000	1.55	0.0035
ABSOR10480L	480000	1.65	0.0045
ABSOR10900A	900000	1.60	0.0040
ABSOR10900H	900000	1.55	0.0035
ABSOR10900L	900000	1.65	0.0045
ABSOR11200A	1200000	1.60	0.0040
ABSOR11200H	1200000	1.65	0.0035
ABSOR11200L	1200000	1.55	0.0045
ABSOR11800A	1800000	1.60	0.0040
ABSOR11800H	1800000	1.55	0.0035
ABSOR11800L	1800000	1.65	0.0045
ABSOR12100A	2100000	1.60	0.0040
ABSOR12100H	2100000	1.55	0.0035
ABSOR12100L	2100000	1.65	0.0045
ABSOR12400A	2400000	1.60	0.0040
ABSOR12400H	2400000	1.55	0.0035
ABSOR12400L	2400000	1.65	0.0045
ABSOR13000A	3000000	1.60	0.0040
ABSOR13000H	3000000	1.55	0.0035
ABSOR13000L	3000000	1.65	0.0045
ABSOR13600A	3600000	1.60	0.0040
ABSOR13600H	3600000	1.55	0.0035
ABSOR13600L	3600000	1.65	0.0045
ABSOR14200A	4200000	1.60	0.0040
ABSOR14200H	4200000	1.55	0.0035

Model	Cooling Capacity	HIR	EIR
ABSOR14200L	4200000	1.65	0.0045
ABSOR20180A	180000	1.00	0.0070
ABSOR20180H	180000	1.00	0.0065
ABSOR20180L	180000	1.00	0.0075
ABSOR20240A	240000	1.00	0.0070
ABSOR20240H	240000	1.00	0.0065
ABSOR20240L	240000	1.00	0.0075
ABSOR20360A	360000	1.00	0.0070
ABSOR20360H	360000	1.00	0.0065
ABSOR20360L	360000	1.00	0.0075
ABSOR20480A	480000	1.00	0.0070
ABSOR20480H	480000	1.00	0.0065
ABSOR20480L	480000	1.00	0.0075
ABSOR20900A	900000	1.00	0.0070
ABSOR20900H	900000	1.00	0.0065
ABSOR20900L	900000	1.00	0.0075
ABSOR21200A	1200000	1.00	0.0070
ABSOR21200H	1200000	1.00	0.0065
ABSOR21200L	1200000	1.00	0.0075
ABSOR21800A	1800000	1.00	0.0070
ABSOR21800H	1800000	1.00	0.0065
ABSOR21800L	1800000	1.00	0.0075
ABSOR22100A	2100000	1.00	0.0070
ABSOR22100H	2100000	1.00	0.0065
ABSOR22100L	2100000	1.00	0.0075
ABSOR22400A	2400000	1.00	0.0070
ABSOR22400H	2400000	1.00	0.0065
ABSOR22400L	2400000	1.00	0.0075
ABSOR23000A	3000000	1.00	0.0070
ABSOR23000H	3000000	1.00	0.0065
ABSOR23000L	3000000	1.00	0.0075
ABSOR23600A	3600000	1.00	0.0070
ABSOR23600H	3600000	1.00	0.0065
ABSOR23600L	3600000	1.00	0.0075
ABSOR24200A	4200000	1.00	0.0070
ABSOR24200H	4200000	1.00	0.0065
ABSOR24200L	4200000	1.00	0.0075
ABSORG0180A	180000	1.00	0.0071
ABSORG0180H	180000	1.00	0.0066
ABSORG0180L	180000	1.00	0.0076

Model	Cooling Capacity	HIR	EIR
ABSORG0240A	240000	1.00	0.0071
ABSORG0240H	240000	1.00	0.0066
ABSORG0240L	240000	1.00	0.0076
ABSORG0360A	360000	1.00	0.0071
ABSORG0360H	360000	1.00	0.0066
ABSORG0360L	360000	1.00	0.0076
ABSORG0480A	480000	1.00	0.0071
ABSORG0480H	480000	1.00	0.0066
ABSORG0480L	480000	1.00	0.0076
ABSORG0900A	900000	1.00	0.0071
ABSORG0900H	900000	1.00	0.0066
ABSORG0900L	900000	1.00	0.0076
ABSORG1200A	1200000	1.00	0.0071
ABSORG1200H	1200000	1.00	0.0066
ABSORG1200L	1200000	1.00	0.0076
ABSORG1800A	1800000	1.00	0.0071
ABSORG1800H	1800000	1.00	0.0066
ABSORG1800L	1800000	1.00	0.0076
ABSORG2100A	2100000	1.00	0.0071
ABSORG2100H	2100000	1.00	0.0066
ABSORG2100L	2100000	1.00	0.0076
ABSORG2400A	2400000	1.00	0.0071
ABSORG2400H	2400000	1.00	0.0066
ABSORG2400L	2400000	1.00	0.0076
ABSORG3000A	3000000	1.00	0.0071
ABSORG3000H	3000000	1.00	0.0066
ABSORG3000L	3000000	1.00	0.0076
ABSORG3600A	3600000	1.00	0.0071
ABSORG3600H	3600000	1.00	0.0066
ABSORG3600L	3600000	1.00	0.0076
ABSORG4200A	4200000	1.00	0.0071
ABSORG4200H	4200000	1.00	0.0066
ABSORG4200L	4200000	1.00	0.0076

Table NF-16– ACM TOWER LIBRARY

Model	CoolCap
TOWER0220	220000
TOWER0260	260000
TOWER0330	330000

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Model	CoolCap
TOWER0390	390000
TOWER0500	500000
TOWER0930	930000
TOWER1250	1250000
TOWER1870	1870000
TOWER2160	2160000
TOWER2480	2480000
TOWER3100	3100000
TOWER3700	3700000
TOWER4300	4300000

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Table NF-17– ACM BOILER LIBRARY

Model	Size	Afue
BOILER00100A	100000	82
BOILER00100H	100000	84
BOILER00100L	100000	80
BOILER00250A	250000	82
BOILER00250H	250000	84
BOILER00250L	250000	80
BOILER00500A	500000	82
BOILER00500H	500000	84
BOILER00500L	500000	80
BOILER00750A	750000	82
BOILER00750H	750000	84
BOILER00750L	750000	80
BOILER01000A	1000000	82
BOILER01000H	1000000	84
BOILER01000L	1000000	80
BOILER01500A	1500000	82
BOILER01500H	1500000	84
BOILER01500L	1500000	80
BOILER02000A	2000000	82
BOILER02000H	2000000	84
BOILER02000L	2000000	80
BOILER02500A	2500000	82
BOILER02500H	2500000	84
BOILER02500L	2500000	80
BOILER03000A	3000000	82
BOILER03000H	3000000	84
BOILER03000L	3000000	80

Table NF-18– ACM VAV BOX SELECTED

Test	System	Zone	Model
A12B13	SYS-1	EAST1	VAV900A
A12B13	SYS-1	EAST2	VAV1200A
A12B13	SYS-1	NORTH1	VAV900A
A12B13	SYS-1	NORTH2	VAV900A
A12B13	SYS-1	SOUTH1	VAV1500A
A12B13	SYS-1	SOUTH2	VAV1500A
A12B13	SYS-1	WEST1	VAV1200A
A12B13	SYS-1	WEST2	VAV1200A
A13B06	SYS-1	EAST1	VAV900A
A13B06	SYS-1	EAST2	VAV1200A
A13B06	SYS-1	NORTH1	VAV600A
A13B06	SYS-1	NORTH2	VAV900A
A13B06	SYS-1	SOUTH1	VAV1200A
A13B06	SYS-1	SOUTH2	VAV1500A
A13B06	SYS-1	WEST1	VAV1200A
A13B06	SYS-1	WEST2	VAV1200A
A14B16	SYS-1	EAST1	VAV900A
A14B16	SYS-1	EAST2	VAV900A
A14B16	SYS-1	NORTH1	VAV600A
A14B16	SYS-1	NORTH2	VAV900A
A14B16	SYS-1	SOUTH1	VAV1200A
A14B16	SYS-1	SOUTH2	VAV1500A
A14B16	SYS-1	WEST1	VAV900A
A14B16	SYS-1	WEST2	VAV1200A
A17B16	SYS-1	EAST1	VAV900A
A17B16	SYS-1	EAST2	VAV900A
A17B16	SYS-1	NORTH1	VAV600A
A17B16	SYS-1	NORTH2	VAV600A
A17B16	SYS-1	SOUTH1	VAV900A
A17B16	SYS-1	SOUTH2	VAV900A
A17B16	SYS-1	WEST1	VAV900A
A17B16	SYS-1	WEST2	VAV900A
B11B13	SYS-1	EAST1	VAV1500L
B11B13	SYS-1	EAST2	VAV2000L
B11B13	SYS-1	NORTH1	VAV1200L
B11B13	SYS-1	NORTH2	VAV1200L
B11B13	SYS-1	SOUTH1	VAV2000L
B11B13	SYS-1	SOUTH2	VAV2000L

Test	System	Zone	Model
B11B13	SYS-1	WEST1	VAV2000L
B11B13	SYS-1	WEST2	VAV2000L
B12B13	SYS-1	EAST1	VAV2000L
B12B13	SYS-1	EAST2	VAV2000L
B12B13	SYS-1	NORTH1	VAV1200L
B12B13	SYS-1	NORTH2	VAV1500L
B12B13	SYS-1	SOUTH1	VAV2000L
B12B13	SYS-1	SOUTH2	VAV2500L
B12B13	SYS-1	WEST1	VAV2000L
B12B13	SYS-1	WEST2	VAV2000L
B13B13	SYS-1	EAST1	VAV2000L
B13B13	SYS-1	EAST2	VAV2000L
B13B13	SYS-1	NORTH1	VAV1200L
B13B13	SYS-1	NORTH2	VAV1200L
B13B13	SYS-1	SOUTH1	VAV2500L
B13B13	SYS-1	SOUTH2	VAV2500L
B13B13	SYS-1	WEST1	VAV2000L
B13B13	SYS-1	WEST2	VAV2500L
B14B06	SYS-1	EAST1	VAV2000H
B14B06	SYS-1	EAST2	VAV2000H
B14B06	SYS-1	NORTH1	VAV1200H
B14B06	SYS-1	NORTH2	VAV1200H
B14B06	SYS-1	SOUTH1	VAV2000H
B14B06	SYS-1	SOUTH2	VAV2500H
B14B06	SYS-1	WEST1	VAV2000H
B14B06	SYS-1	WEST2	VAV2000H
B15B16	SYS-1	EAST1	VAV2000H
B15B16	SYS-1	EAST2	VAV2000H
B15B16	SYS-1	NORTH1	VAV900H
B15B16	SYS-1	NORTH2	VAV1200H
B15B16	SYS-1	SOUTH1	VAV2000H
B15B16	SYS-1	SOUTH2	VAV2500H
B15B16	SYS-1	WEST1	VAV2000H
B15B16	SYS-1	WEST2	VAV2500H
B21B12	SYS-1	EAST1	VAV1500A
B21B12	SYS-1	EAST2	VAV1500A
B21B12	SYS-1	NORTH1	VAV1200A
B21B12	SYS-1	NORTH2	VAV1200A
B21B12	SYS-1	SOUTH1	VAV1500A
B21B12	SYS-1	SOUTH2	VAV2000A

Test	System	Zone	Model
B21B12	SYS-1	WEST1	VAV2000A
B21B12	SYS-1	WEST2	VAV2000A
B22B12	SYS-1	EAST1	VAV1200A
B22B12	SYS-1	EAST2	VAV1200A
B22B12	SYS-1	NORTH1	VAV1200A
B22B12	SYS-1	NORTH2	VAV1200A
B22B12	SYS-1	SOUTH1	VAV1500A
B22B12	SYS-1	SOUTH2	VAV1500A
B22B12	SYS-1	WEST1	VAV1500A
B22B12	SYS-1	WEST2	VAV1500A
B23B12	SYS-1	EAST1	VAV1200A
B23B12	SYS-1	EAST2	VAV1200A
B23B12	SYS-1	NORTH1	VAV900A
B23B12	SYS-1	NORTH2	VAV1200A
B23B12	SYS-1	SOUTH1	VAV1500A
B23B12	SYS-1	SOUTH2	VAV1500A
B23B12	SYS-1	WEST1	VAV1500A
B23B12	SYS-1	WEST2	VAV1500A
B24B03	SYS-1	EAST1	VAV1200A
B24B03	SYS-1	EAST2	VAV1200A
B24B03	SYS-1	NORTH1	VAV900A
B24B03	SYS-1	NORTH2	VAV900A
B24B03	SYS-1	SOUTH1	VAV1200A
B24B03	SYS-1	SOUTH2	VAV1200A
B24B03	SYS-1	WEST1	VAV1200A
B24B03	SYS-1	WEST2	VAV1500A
C21B10	SYS-1	EAST2	VAV2000A
C21B10	SYS-1	NORTH1	VAV1500A
C21B10	SYS-1	NORTH2	VAV1200A
C21B10	SYS-1	SOUTH1	VAV2500A
C21B10	SYS-1	SOUTH2	VAV2500A
C21B10	SYS-1	WEST2	VAV2000A
C21B10	SYS-2	INT1	VAV600A
C21B10	SYS-2	INT2	VAV900A
C22C16	SYS-1	ZONE1E	VAV1500A
C22C16	SYS-1	ZONE1I	VAV900A
C22C16	SYS-1	ZONE1N	VAV1200A
C22C16	SYS-1	ZONE1S	VAV1500A
C22C16	SYS-1	ZONE3I	VAV900A
C22C16	SYS-1	ZONE3S	VAV1200A

Test	System	Zone	Model
C22C16	SYS-2	ZONE1W	VAV1500A
C22C16	SYS-2	ZONE3E	VAV2000A
C22C16	SYS-2	ZONE3N	VAV1200A
C22C16	SYS-2	ZONE3W	VAV2000A
E21B16	SYS-1	EAST1	VAV1200A
E21B16	SYS-1	EAST2	VAV1200A
E21B16	SYS-1	INT1	VAV900A
E21B16	SYS-1	INT2	VAV900A
E21B16	SYS-1	NORTH1	VAV600A
E21B16	SYS-1	NORTH2	VAV900A
E21B16	SYS-1	SOUTH1	VAV1500A
E21B16	SYS-1	SOUTH2	VAV1500A
E21B16	SYS-1	WEST1	VAV1200A
E21B16	SYS-1	WEST2	VAV1200A
E22B16	SYS-1	EAST1	VAV1200A
E22B16	SYS-1	EAST2	VAV1200A
E22B16	SYS-1	INT1	VAV900A
E22B16	SYS-1	INT2	VAV900A
E22B16	SYS-1	NORTH1	VAV900A
E22B16	SYS-1	NORTH2	VAV900A
E22B16	SYS-1	SOUTH1	VAV1500A
E22B16	SYS-1	SOUTH2	VAV1500A
E22B16	SYS-1	WEST1	VAV1200A
E22B16	SYS-1	WEST2	VAV1500A
E23B16	SYS-1	EAST1	VAV1200A
E23B16	SYS-1	EAST2	VAV1200A
E23B16	SYS-1	INT1	VAV900A
E23B16	SYS-1	INT2	VAV1200A
E23B16	SYS-1	NORTH1	VAV900A
E23B16	SYS-1	NORTH2	VAV900A
E23B16	SYS-1	SOUTH1	VAV1500A
E23B16	SYS-1	SOUTH2	VAV1500A
E23B16	SYS-1	WEST1	VAV1500A
E23B16	SYS-1	WEST2	VAV1500A
E24B12	SYS-1	EAST1	VAV1200H
E24B12	SYS-1	EAST2	VAV1200H
E24B12	SYS-1	INT1	VAV900H
E24B12	SYS-1	INT2	VAV900H
E24B12	SYS-1	NORTH1	VAV900H
E24B12	SYS-1	NORTH2	VAV900H

Test	System	Zone	Model
E24B12	SYS-1	SOUTH1	VAV2000H
E24B12	SYS-1	SOUTH2	VAV2000H
E24B12	SYS-1	WEST1	VAV1500H
E24B12	SYS-1	WEST2	VAV2000H
E25B12	SYS-1	EAST1	VAV1200H
E25B12	SYS-1	EAST2	VAV1500H
E25B12	SYS-1	INT1	VAV900H
E25B12	SYS-1	INT2	VAV900H
E25B12	SYS-1	NORTH1	VAV900H
E25B12	SYS-1	NORTH2	VAV1200H
E25B12	SYS-1	SOUTH1	VAV2000H
E25B12	SYS-1	SOUTH2	VAV2000H
E25B12	SYS-1	WEST1	VAV1500H
E25B12	SYS-1	WEST2	VAV2000H
E26B12	SYS-1	EAST1	VAV1500H
E26B12	SYS-1	EAST2	VAV1500H
E26B12	SYS-1	INT1	VAV900H
E26B12	SYS-1	INT2	VAV1200H
E26B12	SYS-1	NORTH1	VAV1200H
E26B12	SYS-1	NORTH2	VAV1200H
E26B12	SYS-1	SOUTH1	VAV2000H
E26B12	SYS-1	SOUTH2	VAV2000H
E26B12	SYS-1	WEST1	VAV1500H
E26B12	SYS-1	WEST2	VAV2000H
F13B12	SYS-1	EAST1	VAV2000H
F13B12	SYS-1	EAST2	VAV2000H
F13B12	SYS-1	NORTH1	VAV1200H
F13B12	SYS-1	NORTH2	VAV1500H
F13B12	SYS-1	SOUTH1	VAV2000H
F13B12	SYS-1	SOUTH2	VAV2500H
F13B12	SYS-1	WEST1	VAV2000H
F13B12	SYS-1	WEST2	VAV2000H
F14B12	SYS-1	EAST1	VAV1500H
F14B12	SYS-1	EAST2	VAV2000H
F14B12	SYS-1	NORTH1	VAV1200H
F14B12	SYS-1	NORTH2	VAV1200H
F14B12	SYS-1	SOUTH1	VAV2000H
F14B12	SYS-1	SOUTH2	VAV2000H
F14B12	SYS-1	WEST1	VAV2000H
F14B12	SYS-1	WEST2	VAV2000H

Test	System	Zone	Model
G15B03	SYS-1	EAST1	VAV3000A
G15B03	SYS-1	EAST2	VAV3500A
G15B03	SYS-1	NORTH1	VAV2000A
G15B03	SYS-1	NORTH2	VAV2000A
G15B03	SYS-1	SOUTH1	VAV3500A
G15B03	SYS-1	SOUTH2	VAV4000A
G15B03	SYS-1	WEST1	VAV3500A
G15B03	SYS-1	WEST2	VAV3500A
G15B03	SYS-2	INT1	VAV300A
G15B03	SYS-2	INT2	VAV450A
G16B16	SYS-1	EAST1	VAV600A
G16B16	SYS-1	EAST2	VAV900A
G16B16	SYS-1	NORTH1	VAV450A
G16B16	SYS-1	NORTH2	VAV450A
G16B16	SYS-1	SOUTH1	VAV900A
G16B16	SYS-1	SOUTH2	VAV900A
G16B16	SYS-1	WEST1	VAV900A
G16B16	SYS-1	WEST2	VAV900A
G16B16	SYS-2	INT1	VAV1200A
G16B16	SYS-2	INT2	VAV1500A
O21B13	SYS-1	EAST1	VAV2000A
O21B13	SYS-1	EAST2	VAV2000A
O21B13	SYS-1	INT1	VAV900A
O21B13	SYS-1	INT2	VAV1200A
O21B13	SYS-1	NORTH1	VAV1200A
O21B13	SYS-1	NORTH2	VAV1500A
O21B13	SYS-1	SOUTH1	VAV2000A
O21B13	SYS-1	SOUTH2	VAV2500A
O21B13	SYS-1	WEST1	VAV2000A
O21B13	SYS-1	WEST2	VAV2000A
O22B13	SYS-1	EAST1	VAV2000A
O22B13	SYS-1	EAST2	VAV2000A
O22B13	SYS-1	INT1	VAV900A
O22B13	SYS-1	INT2	VAV1200A
O22B13	SYS-1	NORTH1	VAV1200A
O22B13	SYS-1	NORTH2	VAV1500A
O22B13	SYS-1	SOUTH1	VAV2000A
O22B13	SYS-1	SOUTH2	VAV2500A
O22B13	SYS-1	WEST1	VAV2000A
O22B13	SYS-1	WEST2	VAV2000A

Test	System	Zone	Model
O23B13	SYS-1	EAST1	VAV2000A
O23B13	SYS-1	EAST2	VAV2000A
O23B13	SYS-1	INT1	VAV900A
O23B13	SYS-1	INT2	VAV1200A
O23B13	SYS-1	NORTH1	VAV1200A
O23B13	SYS-1	NORTH2	VAV1500A
O23B13	SYS-1	SOUTH1	VAV2000A
O23B13	SYS-1	SOUTH2	VAV2500A
O23B13	SYS-1	WEST1	VAV2000A
O23B13	SYS-1	WEST2	VAV2000A
O24B13	SYS-1	EAST1	VAV2000A
O24B13	SYS-1	EAST2	VAV2000A
O24B13	SYS-1	INT1	VAV900A
O24B13	SYS-1	INT2	VAV1200A
O24B13	SYS-1	NORTH1	VAV1200A
O24B13	SYS-1	NORTH2	VAV1500A
O24B13	SYS-1	SOUTH1	VAV2000A
O24B13	SYS-1	SOUTH2	VAV2500A
O24B13	SYS-1	WEST1	VAV2000A
O24B13	SYS-1	WEST2	VAV2000A
O41B13	SYS-1	EAST1	VAV2000L
O41B13	SYS-1	EAST2	VAV2000L
O41B13	SYS-1	INT1	VAV900L
O41B13	SYS-1	INT2	VAV1200L
O41B13	SYS-1	NORTH1	VAV1200L
O41B13	SYS-1	NORTH2	VAV1500L
O41B13	SYS-1	SOUTH1	VAV2000L
O41B13	SYS-1	SOUTH2	VAV2500L
O41B13	SYS-1	WEST1	VAV2000L
O41B13	SYS-1	WEST2	VAV2000L
O61B11	SYS-1	EAST1	VAV2000A
O61B11	SYS-1	EAST2	VAV2000A
O61B11	SYS-1	INT1	VAV900A
O61B11	SYS-1	INT2	VAV1200A
O61B11	SYS-1	NORTH1	VAV1200A
O61B11	SYS-1	NORTH2	VAV1500A
O61B11	SYS-1	SOUTH1	VAV2000A
O61B11	SYS-1	SOUTH2	VAV2500A
O61B11	SYS-1	WEST1	VAV2000A
O61B11	SYS-1	WEST2	VAV2000A



Test	System	Zone	Model
O62B11	SYS-1	EAST1	VAV2000A
O62B11	SYS-1	EAST2	VAV2000A
O62B11	SYS-1	INT1	VAV900A
O62B11	SYS-1	INT2	VAV1200A
O62B11	SYS-1	NORTH1	VAV1200A
O62B11	SYS-1	NORTH2	VAV1500A
O62B11	SYS-1	SOUTH1	VAV2000A
O62B11	SYS-1	SOUTH2	VAV2500A
O62B11	SYS-1	WEST1	VAV2000A
O62B11	SYS-1	WEST2	VAV2000A
O63B11	SYS-1	EAST1	VAV2000A
O63B11	SYS-1	EAST2	VAV2000A
O63B11	SYS-1	INT1	VAV900A
O63B11	SYS-1	INT2	VAV1200A
O63B11	SYS-1	NORTH1	VAV1200A
O63B11	SYS-1	NORTH2	VAV1500A
O63B11	SYS-1	SOUTH1	VAV2000A
O63B11	SYS-1	SOUTH2	VAV2500A
O63B11	SYS-1	WEST1	VAV2000A
O63B11	SYS-1	WEST2	VAV2000A
O64B11	SYS-1	EAST1	VAV2000A
O64B11	SYS-1	EAST2	VAV2000A
O64B11	SYS-1	INT1	VAV900A
O64B11	SYS-1	INT2	VAV1200A
O64B11	SYS-1	NORTH1	VAV1200A
O64B11	SYS-1	NORTH2	VAV1500A
O64B11	SYS-1	SOUTH1	VAV2000A
O64B11	SYS-1	SOUTH2	VAV2500A
O64B11	SYS-1	WEST1	VAV2000A
O64B11	SYS-1	WEST2	VAV2000A
O65B11	SYS-1	EAST1	VAV2000A
O65B11	SYS-1	EAST2	VAV2000A
O65B11	SYS-1	INT1	VAV900A
O65B11	SYS-1	INT2	VAV1200A
O65B11	SYS-1	NORTH1	VAV1200A
O65B11	SYS-1	NORTH2	VAV1500A
O65B11	SYS-1	SOUTH1	VAV2000A
O65B11	SYS-1	SOUTH2	VAV2500A
O65B11	SYS-1	WEST1	VAV2000A
O65B11	SYS-1	WEST2	VAV2000A

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Test	System	Zone	Model
O66B12	SYS-1	EAST1	VAV2000A
O66B12	SYS-1	EAST2	VAV2000A
O66B12	SYS-1	INT1	VAV900A
O66B12	SYS-1	INT2	VAV1200A
O66B12	SYS-1	NORTH1	VAV1200A
O66B12	SYS-1	NORTH2	VAV1500A
O66B12	SYS-1	SOUTH1	VAV2000A
O66B12	SYS-1	SOUTH2	VAV2500A
O66B12	SYS-1	WEST1	VAV2000A
O66B12	SYS-1	WEST2	VAV2000A

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Table NF-19 – ACM PACKAGE UNITS SELECTED

Test	System	Model
A11B13	SYS-1	ACSP34L
A11B13	SYS-2	ACSP34L
A11B13	SYS-3	ACSP34L
A11B13	SYS-4	ACSP34L
A11B13	SYS-5	ACSP34L
A11B13	SYS-6	ACSP34L
A11B13	SYS-7	ACSP34L
A11B13	SYS-8	ACSP34L
A12B13	SYS-1	ACLP025A
A13B06	SYS-1	ACLP020A
A14B16	SYS-1	ACLP020A
A15B03	SYS-1	ACSP28L
A15B03	SYS-2	ACSP28L
A15B03	SYS-3	ACSP28L
A15B03	SYS-4	ACSP28L
A15B03	SYS-5	ACSP28L
A15B03	SYS-6	ACSP28L
A15B03	SYS-7	ACSP28L
A15B03	SYS-8	ACSP28L
A16B13	SYS-1	ACSP28L
A16B13	SYS-2	ACSP28L
A16B13	SYS-3	ACSP28L
A16B13	SYS-4	ACSP28L
A16B13	SYS-5	ACSP28L
A16B13	SYS-6	ACSP28L
A16B13	SYS-7	ACSP28L
A16B13	SYS-8	ACSP28L
A17B16	SYS-1	ACLP015A
B11B13	SYS-1	ACLP040L
B12B13	SYS-1	ACLP040L
B13B13	SYS-1	ACLP040L
B14B06	SYS-1	ACLP040H
B15B16	SYS-1	ACLP040H
B21B12	SYS-1	ACLP030A
B22B12	SYS-1	ACLP025A
B23B12	SYS-1	ACLP030A
B24B03	SYS-1	ACLP025A
B31D12	SYS-1	ACLP007A

Test	System	Model
B32D12	SYS-1	ACLP007A
C11A10	SYS-1	ACLP015A
C12A10	SYS-1	ACLP015A
C13A10	SYS-1	ACLP025A
C14A10	SYS-1	ACLP010A
C15A10	SYS-1	ACLP010A
C21B10	SYS-1	ACLP030A
C21B10	SYS-2	ACSP46A
C21B10	SYS-3	HEAT045A
C21B10	SYS-4	HEAT063A
D11D12	SYS-1	ACSP63A
D12D12	SYS-1	ACSP63A
D13D07	SYS-1	ACSP52A
D14D07	SYS-1	ACSP52A
E11D16	SYS-1	ACSP22A
E12D16	SYS-1	ACSP28A
E13D16	SYS-1	ACSP28A
E14D14	SYS-1	ACSP40A
E15D14	SYS-1	ACSP40A
E16D14	SYS-1	ACSP52A
E21B16	SYS-1	ACLP025A
E22B16	SYS-1	ACLP030A
E23B16	SYS-1	ACLP030A
E24B12	SYS-1	ACLP030H
E25B12	SYS-1	ACLP040H
E26B12	SYS-1	ACLP040H
F13B12	SYS-1	ACLP040H
F14B12	SYS-1	ACLP040H
G11A11	SYS-1	ACLP025A
G12A11	SYS-1	ACLP007A
G15B03	SYS-1	ACLP015A
G15B03	SYS-2	ACLP007A
G16B16	SYS-1	ACLP060A
G16B16	SYS-2	ACSP22A
O31A12	SYS-1	ACLP015A
O32A12	SYS-1	ACLP010H
O33A12	SYS-1	ACLP010H
O41B13	SYS-1	ACLP040L
O81A11	SYS-1	ACLP015A
O82A15	SYS-1	ACLP015A

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Test	System	Model
OC1A09	SYS-1	NOHVAC
OC2A09	SYS-1	NOHVAC
OC3A09	SYS-1	ACLP015H
OC4A09	SYS-1	ACLP010A
OC4A09	SYS-2	ACLP010A

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*Table NF-20 – ACM WATER LOOP HEAT PUMP SELECTED*

Test	System	Zone	Model
O71B12	SYS-1	EAST1	WHP060A
O71B12	SYS-1	EAST2	WHP060A
O71B12	SYS-1	INT1	WHP036A
O71B12	SYS-1	INT2	WHP042A
O71B12	SYS-1	NORTH1	WHP042A
O71B12	SYS-1	NORTH2	WHP042A
O71B12	SYS-1	SOUTH1	WHP072A
O71B12	SYS-1	SOUTH2	WHP072A
O71B12	SYS-1	WEST1	WHP060A
O71B12	SYS-1	WEST2	WHP072A

*Table NF-21 – ACM EVAPORATIVE COOLING EQUIPMENT SELECTED*

Test	System	Model
O91A13	SYS-1	EVAP2500AIB
O92A11	SYS-1	EVAP2500AID
O93A11	SYS-1	EVAP2500AID
O94A13	SYS-1	EVAP2500AID

*Table NF-22 – FAN COIL UNITS SELECTED*

Test	System	Zone	Model
C22C16	SYS-3	ZONE2E	FC035A
C22C16	SYS-3	ZONE2I	FC013A
C22C16	SYS-3	ZONE2N	FC021A
C22C16	SYS-3	ZONE2S	FC056A
C22C16	SYS-3	ZONE2W	FC042A

*Table NF-23 – ACM HEAT PUMP EQUIPMENT SELECTED*

Test	System	Model
F11A07	SYS-1	HPSP126H
F12A13	SYS-1	HPSP162A
G13A11	SYS-1	HPSP222H
G14A11	SYS-1	HPSP90A

Table NF-24 – ACM SYSTEM EQUIPMENT SELECTED

Test	System	Model
C22C16	SYS-1	SYS0250A
C22C16	SYS-2	SYS0250A
O21B13	SYS-1	SYS0500A
O22B13	SYS-1	SYS0500A
O23B13	SYS-1	SYS0500A
O24B13	SYS-1	SYS0500A
O61B11	SYS-1	SYS0625A
O62B11	SYS-1	SYS0625A
O63B11	SYS-1	SYS0625A
O64B11	SYS-1	SYS0625A
O65B11	SYS-1	SYS0625A
O66B12	SYS-1	SYS0500A

Table NF-25 – ACM CENTRAL COOLING EQUIPMENT SELECTED

Test	Model
C22C16	COOL0900A
C22C16	TOWER0930
O21B13	COOL0480A
O21B13	TOWER0930
O22B13	COOL0480A
O22B13	TOWER0930
O23B13	COOL0480A
O23B13	TOWER0930
O24B13	COOL0480A
O24B13	TOWER0930
O61B11	ABSOR10480A
O61B11	TOWER1250
O62B11	ABSOR20480A
O62B11	TOWER0930
O63B11	ABSORG0480A
O63B11	TOWER0930
O64B11	COOL0480A
O64B11	TOWER0930
O65B11	COOL0480A
O65B11	TOWER0930
O66B12	COOL0480A
O66B12	TOWER0930
O71B12	TOWER0220
O71B12	TOWER0930

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Test	Model
O71B12	TOWER4300

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Table NF-26 – ACM BOILER SELECTION

Test	Model
A12B13	BOILER00250A
A13B06	BOILER00250A
A14B16	BOILER00250A
A17B16	BOILER00250A
B11B13	BOILER00500L
B12B13	BOILER00500L
B13B13	BOILER00500L
B14B06	BOILER00250H
B15B16	BOILER00250H
B21B12	BOILER00250A
B22B12	BOILER00250A
B23B12	BOILER00250A
B24B03	BOILER00250A
C21B10	NOBOILER
C22C16	BOILER01000A
E21B16	BOILER00250A
E22B16	BOILER00250A
E23B16	BOILER00500A
E24B12	BOILER00250H
E25B12	BOILER00250H
E26B12	BOILER00250H
F13B12	NOBOILER
F14B12	NOBOILER
G15B03	NOBOILER
G16B16	NOBOILER
O21B13	BOILER00500A
O22B13	BOILER00500A
O23B13	BOILER00500A
O24B13	BOILER00500A
O41B13	BOILER00500L
O61B11	BOILER01500A
O62B11	BOILER00750A
O63B11	BOILER00500A
O64B11	BOILER00500A
O65B11	BOILER00500A
O66B12	BOILER00500A
O71B12	BOILER00500A

## NONRESIDENTIAL ACM MANUAL APPENDIX NG

# Appendix NG - Standard Procedure for Determining the Energy Efficiencies of Single-Zone Nonresidential Air Distribution Systems in Buffer Spaces or Outdoors

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### NG.1 Purpose and Scope

ACM NG contains procedures for measuring the air leakage in single zone, nonresidential air distribution systems and for calculating the annual and hourly duct system efficiency for energy calculations. The methods described here apply to single zone, constant volume heating and air conditioning systems serving zones with 5000 ft<sup>2</sup> of floor area or less, with duct systems located in unconditioned or semi-conditioned buffer spaces or outdoors. These calculations apply to new buildings or new air conditioning systems applied to existing buildings.

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### NG.2 Definitions

**aerosol sealant closure system:** A method of sealing leaks by blowing aerosolized sealant particles into the duct system which must include minute-by-minute documentation of the sealing process.

**buffer space:** an unconditioned or indirectly conditioned space located between a ceiling and the roof.

**cool roof:** a roofing material with high thermal emittance and high solar reflectance, or lower thermal emittance and exceptionally high solar reflectance as specified in Standards § 118 (i) that reduces heat gain through the roof.

**delivery effectiveness:** The ratio of the thermal energy delivered to the conditioned space and the thermal energy entering the distribution system at the equipment heat exchanger.

**distribution system efficiency:** The ratio of the thermal energy consumed by the equipment with the distribution system to the energy consumed if the distribution system had no losses or impact on the equipment or building loads.

**equipment efficiency:** The ratio between the thermal energy entering the distribution system at the equipment heat exchanger and the energy being consumed by the equipment.

**equipment factor :**  $F_{\text{equip}}$  is the ratio of the equipment efficiency including the effects of the distribution system to the equipment efficiency of the equipment in isolation.

**fan flowmeter device:** A device used to measure air flow rates under a range of test pressure differences.

**floor area:** The floor area of enclosed conditioned space on all floors of a building, as measured at the floor level of the exterior surfaces enclosing the conditioned space.

**Flow capture hood:** A device used to capture and measure the airflow at a register.

**load factor :**  $F_{\text{load}}$  is the ratio of the building energy load without including distribution effects to the load including distribution system effects.

**pressure pan :** a device used to seal individual forced air system registers and to measure the static pressure from the register.

**recovery factor :**  $F_{\text{recov}}$  is the fraction of energy lost from the distribution system that enters the conditioned space.

**thermal regain:** The fraction of delivery system losses that are returned to the building.

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### NG.3 Nomenclature

$a_r$  = duct leakage factor (1-return leakage) for return ducts

$a_s$  = duct leakage factor (1-supply leakage) for supply ducts

$A_{\text{duct,buffer}}$  = total supply plus return duct area in buffer space, ft<sup>2</sup>

$A_{\text{duct,outdoor}}$  = total supply plus return duct area located outdoors, ft<sup>2</sup>

$A_{\text{duct,n}}$  = total supply plus return duct area in space n, ft<sup>2</sup>

$A_{\text{floor}}$  = conditioned floor area of building, ft<sup>2</sup>

$A_{r,\text{buffer}}$  = return duct surface area in buffer space, ft<sup>2</sup>

$A_{r,\text{total}}$  = total return duct surface area, ft<sup>2</sup>

$A_{s,\text{buffer}}$  = supply duct surface area in buffer space, ft<sup>2</sup>

$A_{s,\text{total}}$  = total supply duct surface area, ft<sup>2</sup>

$A_{\text{walls}}$  = area of buffer space exterior walls, ft<sup>2</sup>

$A_{\text{roof}}$  = area of buffer space roof, ft<sup>2</sup>

$B_r$  = conduction fraction for return

$B_s$  = conduction fraction for supply

$C_p$  = specific heat of air = 0.24 Btu/(lb·°F)

$C_{DT}, C_{0h}, C_R, C_L$  = regression coefficients for hourly model

DE = delivery effectiveness

DE<sub>seasonal</sub> = seasonal delivery effectiveness

$E_{\text{equip}}$  = rate of energy exchanged between equipment and delivery system, Btu/hour

$E_{hr}$  = hourly HVAC system energy input (kW for electricity, therms for gas)

$F_{\text{cycloss}}$  = cyclic loss factor

$F_{\text{equip}}$  = load factor for equipment

$F_{\text{leak}}$  = fraction of system fan flow that leaks out of supply or return ducts

$F_{\text{load}}$  = load factor for delivery system

$F_{\text{recov}}$  = thermal loss recovery factor

$F_{\text{regain}}$  = thermal regain factor

$h_o$  = outside roof surface convection coefficient, = 3.4 Btu/hr ft<sup>2</sup>°F

$I_{\text{hor}}$  = global solar radiation on horizontal surface, Btu/hr ft<sup>2</sup>

$K_r$  = return duct surface area coefficient

$K_s$  = supply duct surface area coefficient

$N_{\text{story}}$  = number of stories of the building

$P_{\text{sp}}$  = pressure difference between supply plenum and conditioned space [Pa]

$P_{\text{test}}$  = test pressure for duct leakage [Pa]

$Q_{\text{buffer}}$  = buffer space infiltration rate, cfm

$Q_e$  = Flow through air handler at 400 cfm/rated ton with rated tons defined by unit scheduled capacity at the conditions the unit's ARI rating standard from Section 112 of the Standard. Airflow through heating only furnaces shall be based on a 21.7 cfm/kBtuh rated output capacity.

$Q_{\text{total},25}$  = total duct leakage at 25 Pascal, cfm

$R_r$  = thermal resistance of return duct,  $\text{h ft}^2\text{°F/Btu}$

$R_s$  = thermal resistance of supply duct,  $\text{h ft}^2\text{°F/Btu}$

$T_{\text{amb,cool}}$  = cooling season ambient temperature, °F

$T_{\text{amb,heat}}$  = heating season ambient temperature, °F

$T_{\text{amb,r}}$  = ambient temperature for return, °F

$T_{\text{amb,s}}$  = ambient temperature for supply, °F

$T_{\text{in}}$  = temperature of indoor air, °F

$T_{\text{solair}}$  = sol-air temperature, °F

$T_{\text{sp}}$  = supply plenum air temperature, °F

$UA_c$  = UA value for the interface between the conditioned space and the buffer space,  $\text{Btu/°F}$

$UA_{\text{walls}}$  = UA value for the buffer space exterior walls,  $\text{Btu/°F}$

$UA_{\text{roof}}$  = UA value for the buffer space exterior roof,  $\text{Btu/°F}$

$UA_c$  = UA value for the interface between the conditioned space and the buffer space,  $\text{Btu/°F}$

$ZLC_c$  = zone loss coefficient for the interface between the conditioned space and the buffer space,  $\text{Btu/°F}$

$ZLC_{\text{total}}$  = sum of all the zone loss coefficients for the buffer space,  $\text{Btu/°F}$

$\alpha$  = solar absorptivity of roof, = 0.70 for standard roof; 0.45 for cool roof, 0.0 for ducts located outdoors

$\Delta T_e$  = temperature rise across heat exchanger, °F

$\Delta T_r$  = temperature difference between indoors and the ambient for the return, °F

$\Delta T_s$  = temperature difference between indoors and the ambient for the supply, °F

$\Delta T_{\text{sky}}$  = reduction of sol-air temperature due to sky radiation, = 6.5°F for standard roof and cool roof, 0.0°F for ducts located outdoors, °F.

$\Delta T_{\text{sol,hr}}$  = hourly difference between sol-air and indoor temperatures, °F

$\Delta T_{\text{sol, season}}$  = energy weighted seasonal average difference between sol-air and indoor temperatures, °F

$h_{\text{adj,hr}}$  = hourly distribution efficiency adjustment factor

$\eta_{\text{dist,seasonal}}$  = seasonal distribution system efficiency

$h_{\text{dist,hr}}$  = hourly distribution system efficiency

$\rho$  = density of air = 0.075,  $\text{lb/ft}^3$

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## **NG.4 Air Distribution Diagnostic Measurement and Default Assumptions**

### **NG.4.1 Instrumentation Specifications**

The instrumentation for the air distribution diagnostic measurements shall conform to the following specifications:

#### **NG.4.1.1 Pressure Measurements**

All pressure measurements shall be measured with measurement systems (i.e. sensor plus data acquisition system) having an accuracy of  $\pm 0.2$  Pa. All pressure measurements within the duct system shall be made with static pressure probes.

#### **NG.4.1.2 Duct Leakage Measurements**

The measurement of air flows during duct leakage testing shall have an accuracy of  $\pm 3\%$  of measured flow using digital gauges.

All instrumentation used for duct leakage diagnostic measurements shall be calibrated according to the manufacturer's calibration procedure to conform to the above accuracy requirement. All testers performing diagnostic tests shall obtain evidence from the manufacturer that the equipment meets the accuracy specifications. The evidence shall include equipment model, serial number, the name and signature of the person of the test laboratory verifying the accuracy, and the instrument accuracy. All diagnostic testing equipment is subject to re-calibration when the period of the manufacturer's guaranteed accuracy expires.

### **NG.4.2 Apparatus**

#### **NG.4.2.1 Duct Pressurization**

The apparatus for fan pressurization duct leakage measurements shall consist of a duct pressurization and flow measurement device meeting the specifications in Section NG.4.1.2.

### **NG.4.3 Procedure**

The following sections identify input values for building and HVAC system (including ducts) using either default or diagnostic information.

#### **NG.4.3.1 Building Information and Defaults**

The calculation procedure for determining air distribution efficiencies requires the following building information:

1. climate zone for the building,
2. conditioned floor area,
3. number of stories,
4. areas and U-values of surfaces enclosing space between the roof and a ceiling, and
5. surface area of ductwork if ducts are located outdoors or in multiple spaces.

Using default values rather than diagnostic procedures produce relatively low air distribution-system efficiencies. Default values shall be obtained from following sections:

1. the location of the duct system in Section NG.4.3.4,
2. the surface area and insulation level of the ducts in Sections NG.4.3.3, NG.4.3.4 and NG.4.3.6,
3. the system fan flow in Section NG.4.3.7, and

4. the leakage of the duct system in Section NG.4.3.8.

#### **NG.4.3.2 Diagnostic Input**

Diagnostic inputs are used for the calculation of improved duct efficiency. The diagnostics include observation of various duct characteristics and measurement of duct leakage and system fan flows as described in Sections NG.4.3.5 through NG.4.3.8. These observations and measurements replace those assumed as default values.

The diagnostic procedures include:

- Measurement of total duct system leakage as described in Section NG.4.3.8.
- Measurement of duct surface area if ducts are located outdoors or in multiple spaces as described in Section 4.3.3.
- Observation of the insulation level for the supply ( $R_s$ ) and return ( $R_r$ ) ducts outside the conditioned space as described in Section NG.4.3.6.
- Observation of the presence of a cool roof.
- Observation of the presence of an outdoor air economizer.

#### **NG.4.3.3 Duct Surface Area**

The supply-side and return-side duct surface areas shall be calculated separately. If the supply or return duct is located in more than one space, the area of that duct in each space shall be calculated separately. The duct surface area shall be determined using one of the following methods.

##### **NG.4.3.3.1 Default Duct Surface Area**

The default duct surface area for supply and return shall be calculated as follows:

For supplies:

$$\text{Equation NG-1 } A_{s,\text{total}} = K_s A_{\text{floor}}$$

Where  $K_s$  (supply duct surface area coefficient) shall be 0.25 for systems serving the top story only, 0.125 for systems serving the top story plus one other, and 0.08 for systems serving three or more stories.

For returns:

$$\text{Equation NG-2 } A_{r,\text{total}} = K_r A_{\text{floor}}$$

Where  $K_r$  (return duct surface area coefficient) shall be 0.15 for systems serving the top story only, 0.125 for systems serving the top story plus one other, and 0.08 for systems serving three or more stories.

If ducts are located outdoors, the outdoor duct surface area shall be calculated from the duct layout on the plans using measured duct lengths and nominal inside diameters (for round ducts) or inside perimeters (for rectangular ducts) of each outdoor duct run in the building that is within the scope of the calculation procedure. When using the default duct area, outdoor supply duct surface area shall be less than or equal to the default supply duct surface area; outdoor return duct surface area shall be less than or equal to the default return duct surface area.

The surface area of ducts located in the buffer space between ceilings and roofs shall be calculated from:

$$\text{Equation NG-3 } A_{s,\text{buffer}} = A_{s,\text{total}} - A_{s,\text{outdoors}}$$

$$\text{Equation NG-4 } A_{r,\text{buffer}} = A_{r,\text{total}} - A_{r,\text{outdoors}}$$

**NG4.3.3.2 Measured Duct Surface Area**

Measured duct surface areas shall be used when the outdoor duct surface area measured from the plans is greater than default duct surface area for either supply ducts or return ducts. If a duct system passes through multiple spaces that have different ambient temperature conditions as specified in Section 4.3.5, the duct surface area shall be measured for each space individually. The duct surface area shall be calculated from measured duct lengths and nominal inside diameters (for round ducts) or inside perimeters (for rectangular ducts) of each duct run located in buffer spaces or outdoors.

**NG.4.3.4 Duct Location**

Duct systems covered by this procedure are those specified in the Standards § 144(k)3.

**NG.4.3.5 Climate and Duct Ambient Conditions**

Duct ambient temperatures for both heating and cooling shall be obtained from Tables NG-1a to NG-1e. The duct ambient temperatures for the cool roofs from Table NG-1c shall be used for ducts located in unconditioned spaces other than attics and outside. Indoor dry-bulb ( $T_{in}$ ) temperature for cooling is 78°F. The indoor dry-bulb temperature for heating is 70°F.

*Table NG-1a Assumptions for Duct Ceiling/Roof Space Ambient Temperature, Ceiling Insulation, No roof insulation, Non-vented Attic*

Climate zone	Duct Ambient Temperature for Heating, T amb, heat	Duct Ambient Temperature for Cooling, T amb,, cool Standard roof without economizer	Duct Ambient Temperature for Cooling, T amb,, cool Cool roof without economizer	Duct Ambient Temperature for Cooling, T,amb, cool Standard roof with economizer	Duct Ambient Temperature for Cooling, T amb,, cool Cool roof with economizer
1	47.3	78.0	72.4	81.4	75.3
2	41.8	93.2	84.8	97.1	88.2
3	47.8	83.5	77.1	86.6	79.8
4	43.9	89.1	82.0	92.0	84.5
5	46.2	83.8	77.5	86.0	79.3
6	50.8	85.4	79.4	87.3	81.1
7	49.3	86.8	80.7	88.7	82.3
8	47.3	91.3	84.2	93.1	85.9
9	48.7	92.5	85.4	94.4	87.2
10	45.7	95.9	87.9	98.2	90.0
11	43.9	95.5	88.1	98.4	90.5
12	44.2	94.3	86.7	97.3	89.3
13	43.3	100.9	92.5	103.6	94.9
14	37.2	99.0	90.6	102.7	93.8
15	47.2	102.9	95.8	104.3	97.1
16	37.9	92.0	83.8	96.3	87.5



*Table NG-1b Default Assumptions for Duct Ceiling/Roof Space Ambient Temperature, Ceiling Insulation, No roof insulation, Vented Attic*

Climate zone	Duct Ambient Temperature for Heating, $T_{amb, heat}$	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Standard roof without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Cool roof without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Standard roof with economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Cool roof with economizer
1	48.6	73.7	69.8	76.7	72.5
2	43.4	87.9	82.2	91.7	85.7
3	48.9	79.2	74.8	82.1	77.4
4	45.1	84.4	79.5	87.1	81.9
5	47.7	79.7	75.4	81.9	77.3
6	51.8	81.0	76.8	81.0	78.5
7	50.6	82.4	78.1	84.1	79.7
8	48.7	86.4	81.5	88.2	83.2
9	49.3	88.4	83.4	90.2	85.1
10	47.1	90.9	85.4	93.2	87.6
11	44.8	90.9	85.8	93.7	88.3
12	45.2	89.6	84.4	92.5	87.0
13	44.5	95.1	89.3	97.7	91.7
14	38.6	93.7	87.8	97.2	91.0
15	48.4	98.6	93.7	100.1	95.1
16	38.7	86.9	81.1	91.1	84.9

*Table NG-1c Default Assumptions for Duct Ceiling/Roof Space Ambient Temperature, Ceiling Insulation, Roof insulation, Non-vented Attic*

Climate zone	Duct Ambient Temperature for Heating, $T_{amb, heat}$	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Standard roof without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Cool roof without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Standard roof with economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Cool roof with economizer
1	56.4	77.6	74.8	79.9	76.9
2	54.8	86.9	82.8	89.7	85.4
3	56.4	81.1	77.9	83.3	79.9
4	54.6	84.9	81.3	87.0	83.3
5	56.6	81.3	78.2	82.9	79.6
6	57.1	83.9	80.1	85.5	81.6
7	55.7	84.9	81.1	86.5	82.5
8	54.5	88.0	83.6	89.5	85.0
9	59.9	83.6	81.6	84.2	82.1
10	55.9	89.4	85.6	91.2	87.2
11	53.1	89.7	86.1	91.8	87.9
12	53.7	88.7	84.8	90.9	86.8
13	53.6	93.1	89.0	95.2	90.9
14	48.7	91.9	87.6	94.7	90.1
15	56.1	95.9	92.3	97.0	93.4
16	48.5	86.6	82.4	89.6	85.1

*Table NG-1d Default Assumptions for Duct Ceiling/Roof Space Ambient Temperature, Roof Insulation, No Ceiling Insulation, Non-vented Attic*

Climate zone	Duct Ambient Temperature for Heating, $T_{amb, heat}$	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Standard roof without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Cool roof without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Standard roof with economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Cool roof with economizer
1	59.8	78.5	77.3	79.3	78.0
2	59.0	82.5	80.8	83.5	81.6
3	60.1	80.0	78.6	80.7	79.3
4	58.9	81.6	80.1	82.3	80.7
5	60.0	80.0	78.6	80.6	79.1
6	60.4	81.2	79.5	81.8	80.0
7	59.7	81.7	79.9	82.2	80.5
8	58.8	83.1	81.1	83.7	81.7
9	59.9	83.6	81.6	84.2	82.1
10	58.5	83.4	81.8	84.0	82.3
11	58.5	83.7	82.1	84.3	82.7
12	58.3	83.2	81.6	83.8	82.1
13	58.3	85.1	83.3	85.7	83.9
14	54.5	84.5	82.8	85.4	83.5
15	58.6	86.1	84.6	86.5	84.9
16	55.6	82.4	80.7	83.4	81.5

Table NG-1e Default Assumptions for Duct Ambient Temperature, Ducts Located Outdoors

Climate zone	Duct Ambient Temperature for Heating, $T_{amb, heat}$	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ Without economizer	Duct Ambient Temperature for Cooling, $T_{amb, cool}$ With economizer
1	47.7	62.7	65.4
2	42.5	76.0	79.7
3	47.6	68.5	71.3
4	43.5	73.3	75.8
5	47.1	69.5	71.7
6	50.7	70.0	71.8
7	50.2	71.6	73.2
8	48.3	74.6	76.4
9	47.0	78.1	80.0
10	46.7	79.9	82.1
11	42.8	81.3	83.8
12	43.4	79.4	82.0
13	43.0	83.2	85.4
14	36.4	81.8	85.1
15	48.1	90.7	92.2
16	35.7	73.5	78.1

**NG.4.3.6 Duct Wall Thermal Resistance****NG.4.3.6.1 Default Duct Insulation R value**

Default duct wall thermal resistance for new buildings is R-8.0, the mandatory requirement for ducts installed in newly constructed buildings, additions and new or replacement ducts installed in existing buildings. Default duct wall thermal resistance for existing ducts in existing buildings is R-4.2. An air film resistance of 0.7 [h ft<sup>2</sup> °F/BTU] shall be added to the duct insulation R value to account for external and internal film resistance.

**NG.4.3.6.2 Diagnostic Duct Wall Thermal Resistance**

Duct wall thermal resistance shall be determined from the manufacturer's specification observed during diagnostic inspection. If ducts with multiple R values are installed, the lowest duct R value shall be used. If a duct with a higher R value than 8.0 is installed, the R-value shall be clearly stated on the building plans and a visual inspection of the ducts must be performed to verify the insulation values.

**NG.4.3.7 Total Fan Flow**

The total fan flow for an air conditioner or a heat pump for **all climate zones** shall be equal to 400 cfm/rated ton with rated tons defined by unit scheduled capacity at the conditions the unit's ARI rating standard from Section 112 of the Standard. Airflow through heating only furnaces shall be based on 21.7 cfm/kBtuh rated output capacity.

**NG.4.3.8 Duct Leakage****NG.4.3.8.1 Duct Leakage Factor for Delivery Effectiveness Calculations**

Default duct leakage factors for the Proposed Design shall be obtained from Table NG-2, using the “not Tested” values.

Duct leakage factors for the Standard Design shall be obtained from Table NG-2, using the appropriate “Tested” value.

Duct leakage factors shown in Table NG-2 shall be used in calculations of delivery effectiveness.

*Table NG-2 Duct Leakage Factors*

	as = ar =
Untested duct systems	0.82
Sealed and tested duct systems in existing buildings, System tested after HVAC equipment and/or duct installation	0.915
Sealed and tested new duct systems. System tested after HVAC system installation	0.96

#### *NG.4.3.8.2 Diagnostic Duct Leakage*

Diagnostic duct leakage measurement is used by installers and raters to verify that total leakage meets the criteria for any sealed duct system specified in the compliance documents. Table NG-3 shows the leakage criteria and test procedures that may be used to demonstrate compliance. In addition to the minimum tests shown, existing duct systems may be tested to show they comply with the criteria for new duct systems.

*Table NG-3 Duct Leakage Tests*

Case	User and Application	Leakage criteria, % of total fan flow	Procedure
Sealed and tested new duct systems	Installer Testing HERS Rater Testing	6%	NG 4.3.8.2.1
Sealed and tested altered existing duct systems	Installer Testing HERS Rater Testing	15% Total Duct Leakage	NG 4.3.8.2.1
	Installer Testing and Inspection HERS Rater Testing and Verification	60% Reduction in Leakage and Visual Inspection	NG 4.3.8.2.2 RC4.3.6 and RC4.3.7
	Installer Testing and Inspection HERS Rater Testing and Verification	Fails Leakage Test but All Accessible Ducts are Sealed And Visual Inspection	NG 4.3.8.2.3 RC4.3.6 and RC4.3.7

#### *NG.4.3.8.2.1 Total Duct Leakage Test from Fan Pressurization of Ducts*

The objective of this procedure is for an installer to determine or a rater to verify the total leakage of a new or altered duct system. The total duct leakage shall be determined by pressurizing both the supply and return ducts to 25 Pascals with all ceiling diffusers/grilles and HVAC equipment installed. When existing ducts are to be altered, this test shall be performed prior to and after duct sealing. The following procedure shall be used for the fan pressurization tests:

1. Verify that the air handler, supply and return plenums and all the connectors, transition pieces, duct boots and registers are installed. The entire system shall be included in the test.
2. For newly installed or altered ducts, verify that cloth backed rubber adhesive duct tape has not been used.

3. Seal all the supply and return registers, except for one return register or the system fan access. Verify that all outside air dampers and /or economizers are sealed prior to pressurizing the system.
2. Attach the fan flowmeter device to the duct system at the unsealed register or access door.
3. Install a static pressure probe at a supply.
4. Adjust the fan flowmeter to produce a 25 Pascal (0.1 in water) pressure difference between the supply duct and the outside or the building space with the entry door open to the outside.
5. Record the flow through the flowmeter ( $Q_{\text{total},25}$ ) - this is the total duct leakage flow at 25 Pascals.
6. Divide the leakage flow by the total fan flow and convert to a percentage. If the leakage flow percentage is less than 6% for new duct systems or less than 15% for altered duct systems, the system passes.

Duct systems that have passed this total leakage test will be sampled by a HERS rater to show compliance.

#### *NG 4.3.8.2.2 Leakage Improvement from Fan Pressurization of Ducts*

For altered existing duct systems which have a higher leakage percentage than the Total Duct leakage criteria in Section NG 4.3.8.2.1, the objective of this test is to show that the original leakage is reduced through duct sealing as specified in Table NG-3. The following procedure shall be used:

1. Use the procedure in NG 4.3.8.2.1 to measure the leakage before commencing duct sealing.
2. After sealing is complete use the same procedure to measure the leakage after duct sealing.
3. Subtract the sealed leakage from the original leakage and divide the remainder by the original leakage. If the leakage reduction is 60% or greater of the original leakage, the system passes.
4. Complete the Visual Inspection specified in NG 4.3.8.2.4.

Duct systems that have passed this leakage reduction test and the visual inspection test will be sampled by a HERS rater to show compliance.

#### *NG 4.3.8.2.3 Sealing of All Accessible Leaks*

For altered existing duct systems that do not pass the Total Leakage test (NG 4.3.8.2.1), the objective of this test is to show that all accessible leaks are sealed and that excessively damaged ducts have been replaced. The following procedure shall be used:

1. Complete each of the leakage tests
1. Complete the Visual Inspection as specified in NG 4.3.8.2.4.

All duct systems that could not pass either the total leakage test or the leakage improvement test will be tested by a HERS rater to show compliance. This is a sampling rate of 100%.

#### *NG 4.3.8.2.4 Visual Inspection of Accessible Duct Sealing*

For altered existing duct systems that fail to be sealed to 15% of total fan flow, the objective of this inspection is to confirm that all accessible leaks have been sealed and that excessively damaged ducts have been replaced. The following procedure shall be used:

1. Visually inspect to verify that the following locations have been sealed:
  - Connections to plenums and other connections to the forced air unit
  - Refrigerant line and other penetrations into the forced air unit
  - Air handler door panel (do not use permanent sealing material, metal tape is acceptable)
  - Register boots sealed to surrounding material
  - Connections between lengths of duct, as well as connections to takeoffs, wyes, tees, and splitter boxes.

2. Visually inspect to verify that portions of the duct system that are excessively damaged have been replaced. Ducts that are considered to be excessively damaged are:

- Flex ducts with the vapor barrier split or cracked with a total linear split or crack length greater than 12 inches
- Crushed ducts where cross-sectional area is reduced by 30% or more
- Metal ducts with rust or corrosion resulting in leaks greater than 2 inches in any dimension
- Ducts that have been subject to animal infestation resulting in leaks greater than 2 inches in any dimension

#### NG 4.3.8.4 Labeling requirements for tested systems

A sticker shall be affixed to the exterior surface of the air handler access door with the following text in 14 point font:

"The leakage of the air distribution ducts was found to be \_\_\_\_\_ CFM @ 25 Pascals or \_\_\_\_\_ % of total fan flow.

This system (check one):

• Has a leakage rate that is **equal to or lower** than the prescriptive requirement of 6% leakage for new duct systems or 15% leakage for alterations to existing systems. It meets the prescriptive requirements of California Title 24 Energy Efficiency Standards.

• Has a leakage rate **higher than** 6% leakage for new duct systems or 15% leakage for altered existing systems. It does NOT meet the meet or exceed the prescriptive requirements of the Title 24 standards. However, all accessible ducts were sealed.

Signed: \_\_\_\_\_

Print name: \_\_\_\_\_

Print Company Name: \_\_\_\_\_

Print Contractor License No: \_\_\_\_\_

Print Contractor Phone No: \_\_\_\_\_

Do not remove sticker"

### NG.4.4 Delivery Effectiveness (DE) Calculations

Seasonal delivery effectiveness shall be calculated using the seasonal design temperatures from Table NG-1.

#### NG.4.4.1 Calculation of Duct Zone Temperatures

The temperatures of the duct zones outside the conditioned space are determined in Section NG.4.3.5 for seasonal conditions for both heating and cooling.

For heating:

**Equation NG-5**  $T_{amb, s} = T_{amb, r} = T_{amb, heat}$

For cooling:

**Equation NG-6**  $T_{amb, s} = T_{amb, r} = T_{amb, cool}$

Where

$T_{amb, heat}$  and  $T_{amb, cool}$  are determined from values in Table NG.4.1.

If the ducts are not all in the same location, the duct ambient temperature for use in the delivery effectiveness and distribution system efficiency calculations shall be determined using an area weighted average of the duct ambient temperatures for heating and cooling:

$$\text{Equation NG-7 } T_{\text{amb,heat}} = \frac{A_{\text{duct,buffer}} \times T_{\text{ambheat,buffer}} + A_{\text{duct,outdoors}} \times T_{\text{ambheat,outdoors}}}{A_{\text{duct,buffer}} + A_{\text{duct,outdoors}}}$$

$$\text{Equation NG-8 } T_{\text{amb,cool}} = \frac{A_{\text{duct,buffer}} \times T_{\text{ambcool,buffer}} + A_{\text{duct,outdoors}} \times T_{\text{ambcool,outdoors}}}{A_{\text{duct,buffer}} + A_{\text{duct,outdoors}}}$$

where the buffer space ambient temperature shall correspond to the location yielding the lowest seasonal delivery effectiveness.

Alternatively, the duct ambient temperature for use in the delivery effectiveness and distribution system efficiency calculations can be determined using an area weighted average of the duct zone temperatures for heating and cooling in all spaces:

$$\text{Equation NG-9 } T_{\text{amb,heat}} = \frac{A_{\text{duct},1} \times T_{\text{ambheat},1} + A_{\text{duct},2} \times T_{\text{ambheat},2} + \dots + A_n \times T_{\text{ambheat},n}}{A_{\text{duct},1} + A_{\text{duct},2} + \dots + A_{\text{duct},n}}$$

$$\text{Equation NG-10 } T_{\text{amb,cool}} = \frac{A_{\text{duct},1} \times T_{\text{ambcool},1} + A_{\text{duct},2} \times T_{\text{ambcool},2} + \dots + A_n \times T_{\text{ambcool},n}}{A_{\text{duct},1} + A_{\text{duct},2} + \dots + A_{\text{duct},n}}$$

#### NG.4.4.2 Seasonal Delivery Effectiveness (DE)

The supply and return conduction fractions,  $B_s$  and  $B_r$ , shall be calculated as follows:

$$\text{Equation NG-11 } B_s = \exp\left(\frac{-A_{s,\text{out}}}{1.08 Q_e R_s}\right)$$

$$\text{Equation NG-12 } B_r = \exp\left(\frac{-A_{r,\text{out}}}{1.08 Q_e R_r}\right)$$

The temperature difference across the heat exchanger in the following equation is used:

for heating:

$$\text{Equation NG-13 } \Delta T_e = 55$$

for cooling:

$$\text{Equation NG-14 } \Delta T_e = -20$$

The temperature difference between the building conditioned space and the ambient temperature surrounding the supply,  $\Delta T_s$ , and return,  $\Delta T_r$ , shall be calculated using the indoor and the duct ambient temperatures.

$$\text{Equation NG-15 } \Delta T_s = T_{\text{in}} - T_{\text{amb},s}$$

$$\text{Equation NG-16 } \Delta T_r = T_{\text{in}} - T_{\text{amb},r}$$



The seasonal delivery effectiveness for heating or cooling systems shall be calculated using:

$$\text{Equation NG-17} \quad DE_{\text{seasonal}} = a_s B_s - a_s B_s (1 - B_{\text{rar}}) \frac{\Delta T_r}{\Delta T_e} - a_s (1 - B_s) \frac{\Delta T_s}{\Delta T_e}$$

#### NG.4.5 Seasonal Distribution System Efficiency

Seasonal distribution system efficiency shall be calculated using delivery effectiveness, equipment, load, and recovery factors calculated for seasonal conditions.

##### NG.4.5.1 Equipment Efficiency Factor ( $F_{\text{equip}}$ )

$F_{\text{equip}}$  is 1.

##### NG.4.5.2 Thermal Regain ( $F_{\text{regain}}$ )

The reduction in building load due to regain of duct losses shall be calculated using the thermal regain factor.

$$\text{Equation NG-18} \quad F_{\text{regain}} = \frac{ZLC_c}{ZLC_{\text{total}}}$$

where:

$$\text{Equation NG-19} \quad ZLC_c = UA_c + 60Q_e(1 - a_r)rCp$$

$$\text{Equation NG-20} \quad ZLC_{\text{total}} = \sum_{\text{buffer spaces surfaces}} UA + Q_{\text{buffer}} rCp + 60Q_e(1 - a_r)rCp$$

$$\text{Equation NG-21} \quad UA_{\text{buffer spaces surfaces}} = UA_c + UA_{\text{walls}} + UA_{\text{roof}}$$

$$\text{Equation NG-22} \quad Q_{\text{buffer}} = 0.038(60)A_{\text{walls}}rCp \text{ for non-vented buffer spaces}$$

$$\text{Equation NG-23} \quad Q_{\text{buffer}} = 0.25(60)A_{\text{roof}}rCp \text{ for -vented buffer spaces}$$

Thermal regain for ducts located outdoors shall be equal to 0.0. If the ducts are not all in the same location, the regain shall be determined using an area weighted average of the regain for heating and cooling:

$$\text{Equation NG-24} \quad F_{\text{regain}} = \frac{A_{\text{duct},1} \times F_{\text{regain},1} + A_{\text{duct},2} \times F_{\text{regain},2} + \dots + A_{\text{duct},n} \times F_{\text{regain},n}}{A_{\text{duct},1} + A_{\text{duct},2} + \dots + A_{\text{duct},n}}$$

##### NG.4.5.3 Recovery Factor ( $F_{\text{recov}}$ )

The recovery factor,  $F_{\text{recov}}$ , is calculated based on the thermal regain factor,  $F_{\text{regain}}$ , and the duct losses without return leakage.

$$\text{Equation NG-25} \quad F_{\text{recov}} = 1 + F_{\text{regain}} \left( \frac{1 - a_s B_s + a_s B_s (1 - B_r) \frac{\Delta T_r}{\Delta T_e} + a_s (1 - B_s) \frac{\Delta T_s}{\Delta T_e}}{DE_{\text{seasonal}}} \right)$$

**NG.4.5.4 Seasonal Distribution System Efficiency**

The seasonal distribution system efficiency shall be calculated using the seasonal delivery effectiveness from section NG.4.4.2, the equipment efficiency factor from section NG.4.5.1, and the recovery factor from section NG.4.5.3. Note that  $DE_{seasonal}$ ,  $F_{equip}$ ,  $F_{recov}$  must be calculated separately for cooling and heating conditions. Distribution system efficiency shall be determined using the following equation:

$$\text{Equation NG-26} \quad h_{distseasonal} = 0.98 DE_{seasonal} F_{equip} F_{recov}$$

where 0.98 accounts for the energy losses from heating and cooling the duct thermal mass.

**NG.4.6 Hourly Distribution System Efficiency**

The hourly duct efficiency shall be calculated for each hour using the following equation:

$$\text{Equation NG-27} \quad h_{dist,hr} = \frac{h_{dist,seasonal}}{h_{adj,hr}}, \eta_{dist,hr} \leq 1$$

where the hourly efficiency is calculated from the seasonal efficiency and an hourly efficiency adjustment factor. The hourly distribution efficiency shall be less than or equal to 1.0. The hourly duct efficiency adjustment factor shall be calculated from the following equation:

$$\text{Equation NG-28} \quad h_{adj,hr} = 1 + C_{DT} \times (\Delta T_{sol,hr} - \Delta T_{sol,season})$$

where the hourly efficiency adjustment factor is calculated from the difference between the hourly roof sol-air temperature and the hourly indoor temperature; the difference between the seasonal average difference between the roof sol-air temperature and the indoor temperature; and a constant derived from regression analysis.

The hourly difference between the roof sol-air temperature and the indoor temperature shall be calculated from the following equation:

$$\text{Equation NG-29} \quad \Delta T_{sol,hr} = T_{solair,hr} - T_{in,hr}$$

The seasonal difference between the roof sol-air temperature and the indoor temperature shall be a load-weighted average of the hourly roof sol-air temperature and the indoor temperature, and shall be calculated from the following equation:

$$\text{Equation NG-30} \quad \Delta T_{sol,season} = \frac{\sum_{season} (T_{solair,hr} - T_{in,hr}) E_{hr}}{\sum_{season} E_{hr}}$$

The hourly roof sol-air temperature is a function of the hourly ambient temperature, hourly horizontal solar radiation and the roof surface absorptance; and shall be calculated from the following equation:

$$\text{Equation NG-31} \quad T_{solair,hr} = T_{amb,hr} + \left( \frac{a}{h_o} \right) I_{hor,hr} - \Delta T_{sky}$$

The hourly efficiency adjustment factor regression coefficient shall be calculated from the following equation:

**Equation NG-32** 
$$C_{DT} = C_o + \frac{C_R}{R_s} + C_L Q_{total,25}; C_{DT,cooling} \geq 0.0; C_{DT,heating} \leq 0.0$$

where coefficients  $C_o$ ,  $C_R$ , and  $C_L$  shall be taken from Table NG-3 according to the season (heating or cooling), and the roof type for ducts in the buffer space (Standard or Cool roof) or duct location (if outdoors). The calculated value of  $C_{DT}$  for cooling shall be greater than or equal to zero, and the calculated value of  $C_{DT}$  for heating shall be less than or equal to zero.

#### NG.4.6.3 Hourly Efficiency Adjustment Regression Coefficients

Table NG-4 Coefficients

	Cooling			Heating		
	Standard roof	Cool roof	Outdoors	Standard roof	Cool roof	Outdoors
Co	0.000486	0.000538	-0.002763	-0.000430	-0.000418	0.000677
CR	0.002810	0.003207	0.008702	-0.003978	-0.003659	-0.002614
CL	0.002143	0.003386	0.031009	-0.012079	-0.011277	-0.012190

**NONRESIDENTIAL ACM MANUAL APPENDIX NH****Appendix NH - Test Nonresidential Air Distribution Systems**

CASE CODE	Input Assumptions for Non-Residential Duct Systems		
	Total duct Leakage, %	Supply duct R Value	Return duct R value
1001	22	4.2	4.2
1002	22	8	8
1003	8	4.2	4.2
1004	8	8	8

# NONRESIDENTIAL ACM MANUAL APPENDIX NI

## Appendix NI - Alternate Default Fenestration Thermal Properties

### Scope

This appendix applies to fenestration excepted from Section 116 (a) 2 and Section 116 (a) 3 of the Standard.

***“EXCEPTION to Section 116 (a) 2: If the fenestration product is site-built fenestration in a building covered by the nonresidential standards with less than 10,000 square feet of site-built fenestration or is a skylight, the default U-factor may be the applicable U-factor as set forth in the Nonresidential ACM Manual.”***

***“EXCEPTION to Section 116 (a) 3: If the fenestration product is site-built fenestration in a building covered by the nonresidential standards with less than 10,000 square feet of site-built fenestration or is a skylight, the default SHGC may be calculated according to Equation 116-A.”***

### Purpose

To present alternate default U-factors and the calculation method for determining an alternate default SHGC, and to describe the responsibilities of energy consultants, designers, architects, builders, installers, and building departments when an alternate default value is used for determining compliance.

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### NI.1 Solar Heat Gain Coefficient

This section describes the alternative calculation method for determining compliance for eligible site-built products. The following equation may be used to calculate the fenestration product's SHGC used to determine compliance. Convert the center of glass SHGC,  $SHGC_c$ , from the manufacturer's documentation to a value for the fenestration product with framing,  $SHGC_{fen}$ .

$$SHGC_{fen} = 0.08 + 0.86 \times SHGC_c$$

Where:

$SHGC_{fen}$  is the SHGC for the fenestration including glass and frame.

$SHGC_c$  is the SHGC for the center of glass alone, and

### NI.1.2 Responsibilities for SHGC Compliance

This section describes the responsibilities of energy consultants, designers, architects, builders, installers, and building departments when this alternative calculation method is used for determining compliance with SHGC requirements.

#### NI.1.2.1 Energy Consultants, Designers, Architects

##### *Site-Built Fenestration Products without SHGC Rated Using NFRC Procedures*

The procedure described below applies only to skylights and to site-built fenestration in buildings with less than 10,000 ft<sup>2</sup> of site-built fenestration.

To determine compliance with the efficiency standards, the center of glass SHGC from the manufacturer's documentation for the proposed glazing must be converted to an SHGC<sub>fen</sub> for the fenestration that includes the framing effect.

For the Prescriptive compliance method, the SHGC<sub>fen</sub> is then entered into the prescriptive ENV-1 form, Part 2 of 2 and must appear on the building plans.

For the Performance compliance method, the SHGC<sub>fen</sub> output information printed on the Performance ENV-1 form must be listed on the building plans. The PERF-1 and Performance ENV-1 forms must appear on the plans. The building plan window schedule list must indicate the proposed total SHGC<sub>fen</sub> values for each fenestration assembly, and these values must be equal to the SHGCs listed on the Performance ENV-1 computer form. (Note: an under-calculation of space conditioning energy can result from entering either too low or too high an SHGC<sub>fen</sub> for the product.)

Permit applications must include heat gain documentation for the Building Plan Checker. This documentation must include a copy of the manufacturer's documentation showing the SHGC<sub>c</sub>, center of glass alone and the calculation used to determine the SHGC<sub>fen</sub>. If the proposed design uses multiple fenestration products or site-assembled fenestration products, a calculation for each different SHGC<sub>fen</sub> must be attached to the plans along with each glass unit manufacturer's documentation.

Building plans shall identify all site-built fenestration and all site-built fenestration without SHGCs rated using NFRC procedures.

#### *Mixed Fenestration Types*

If mixed fenestration is included in the compliance analysis, then the compliance submittal must demonstrate which are certified fenestration products and which are non-certified fenestration or site-built fenestration products. The manufacturer's documentation and calculations for each product must be included in the submittal, and either the ENV-1 or PERF-1 form must be included on the building plans.

#### **NI.1.2.2 Builder and Installer Responsibilities**

The builder is responsible for ensuring that the glass documentation showing the SHGC used for determining compliance is provided to the installer. The builder is responsible for obtaining an NFRC Label Certificate for Site-Built Products for the building's site-built fenestration if the building has 10,000 ft<sup>2</sup> or more of site-built fenestration.

The builder is also responsible for ensuring that the persons preparing compliance documentation are specifying products that the builder intends to install. The builder must ensure that the glazing contractor installs the glass with the same SHGC<sub>c</sub> as used for compliance and that the building inspector is provided with manufacturers' documentation showing the SHGC<sub>c</sub> for the actual glass product installed. The builder should verify that these fenestration products are clearly shown on the building plans before fenestration products are purchased and installed.

#### **NI.1.2.3 Building Department Responsibilities**

##### *Plan Checker*

The building department plan checker is responsible for ensuring that the plans identify all site-built fenestration.

The plan-checker is responsible for verifying that for skylights and site-built fenestration using the alternate default SHGC calculation:

1. the SHGC<sub>fen</sub> and SHGC<sub>c</sub> are identified on the plans,
2. calculations have been provided showing the conversion from SHGC<sub>c</sub> to SHGC<sub>fen</sub>,
3. manufacturer documentation of the SHGC<sub>c</sub> has been provided for each of the fenestration products using alternate default SHGC calculations, and

4. the building has less than 10,000 ft<sup>2</sup> of site-built fenestration.

Plans should be consistent with the compliance documentation, the calculations showing the conversion from SHGC<sub>c</sub> to SHGC<sub>fen</sub>, and Prescriptive ENV-1 Part 2 of 2 or Performance ENV-1.

#### *Building Inspector*

The building department field inspector is responsible for ensuring that the building using an alternate default SHGC calculation has less than 10,000 ft<sup>2</sup> of site-built fenestration.

The field inspector is responsible for ensuring that the SHGC<sub>c</sub> and SHGC<sub>fen</sub> for the installed fenestration is consistent with the plans, the Prescriptive ENV-1 Part 2 of 2 or the Performance PERF-1 and Performance ENV-1, and that manufacturer documentation is consistent with the product installed in the building.

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## **NI.2 Thermal Transmittance (U-Factor)**

Table NI-1 provides default U-factors for skylights and for site-built fenestration in buildings with less than 10,000 ft<sup>2</sup> of site-built fenestration.

The default Table NI-1 is consistent with default U-factors published in Table 4, Chapter 30, ASHRAE Fundamentals Handbook, 2001, which is referenced in the Energy Standards. Fenestration products fitting the two descriptions above may still use U-factors obtained through NFRC if available.

### **NI.2.1 Responsibilities for U-factor Compliance**

This section describes the responsibilities of energy consultants, designers, architects, builders, installers, and building departments when Table NI-1 is used for determining compliance with the U-factor requirements of the Efficiency Standards.

#### **NI.2.1.1 Energy Consultants, Designers, Architects**

##### *Site-Built Fenestration without U-factor Rated Using NFRC Procedures*

The procedure described below applies only to skylights and to site-built fenestration in buildings with less than 10,000 ft<sup>2</sup> of site-built fenestration. To determine compliance with the efficiency standards, the Glazing Type and Frame Type shown in Table NI-1 must be identified from the manufacturer's documentation for the proposed glazing.

For the Prescriptive compliance method, the U-factor must be selected from Table NI-1 for this Glazing Type and Frame Type and entered into the prescriptive ENV-1 form, Part 2 of 2, and must appear on the building plans.

For the Performance compliance method, the U-factor output information printed on the Performance ENV-1 form must be listed on the building plans. The PERF-1 and Performance ENV-1 forms must appear on the plans. The building plan window schedule list must indicate the proposed total U-factors for each fenestration assembly, and these values must be equal to or less than the U-factors listed on the Performance ENV-1 computer form.

Permit applications must include fenestration U-factor documentation for the Building Plan Checker. This documentation must include a copy of the manufacturer's documentation showing the Glazing Type information – number of panes, spacing of panes, glass type, gas fill type, coating emissivity and location – and the Frame Type – frame material type, presence of thermal breaks, and identification of structural glazing (glazing with no frame) that is used to determine the U-factor. If the proposed design uses multiple fenestration products or site-assembled fenestration products, manufacturer's documentation for each different U-factor for each glass unit must be attached to the plans. Manufacturer's documentation must be provided for each U-factor used for compliance.

Building plans shall identify all site-built fenestration and all site-built fenestration without U-factors rated using NFRC procedures.

#### *Mixed Fenestration Types*

If mixed fenestration is included in the compliance analysis, then the compliance submittal must demonstrate which are certified fenestration products and which are non-certified fenestration or site-assembled fenestration products. The manufacturer's documentation and calculations for each product must be included in the submittal, and either the ENV-1 or PERF-1 form must be included on the building plans.

#### **NI.2.1.2 Builder and Installer Responsibilities**

The builder is responsible for ensuring that the glass documentation showing the U-factor used for determining compliance is provided to the installer. The builder is responsible for ensuring that the persons preparing compliance documentation are specifying products that the builder intends to install. The builder is also responsible for ensuring that the installer installs glass with U-factors the same or lower than the U-factors used for compliance and ensuring that the field inspector for the building department is provided with manufacturer's documentation showing the U-factor and method of determining U-factor for the actual fenestration product installed. The builder should verify that these fenestration products are clearly shown on the building plans before fenestration products are purchased and installed.

#### **NI.2.1.3 Building Department Responsibilities**

##### *Plan Checker*

The building department plan checker is responsible for ensuring that the plans identify all site-built fenestration.

The plan checker shall ensure that for skylights and site-built fenestration using alternate default U-factors:

1. U-factors are identified on the plans,
2. the Glazing Type and Frame Type and Table NI-1 have been provided documenting the method of determining the U-factor,
3. manufacturer documentation of the Glazing Type and Frame Type has been provided for the each of the fenestration products using alternate default U-factors, and
4. the building has less than 10,000 ft<sup>2</sup> of site-built fenestration.

Plans should be consistent with the compliance documentation, the Glazing Type and Frame Type and Table NI-1 values, and Prescriptive ENV-1 Part 2 of 2 or Performance ENV-1.

##### *Building Inspector*

The building department field inspector is responsible for ensuring that the building using an alternate default U-factor has less than 10,000 ft<sup>2</sup> of site-built fenestration.

The building department field inspector is responsible for ensuring that manufacturer's documentation has been provided for the installed fenestration. The field inspector is responsible for ensuring that the U-factor for the installed fenestration is consistent with the plans, the Prescriptive ENV-1 Part 2 of 2 or the Performance PERF-1, and Performance ENV-1, and that manufacturer documentation is consistent with the product installed in the building.



Table NI-1 – Alternate U-Factors for Skylights and Eligible<sup>1</sup> Site-Built Fenestration

Product Type		Vertical Installation				Sloped Installation						
		Unlabeled Glazed Wall Systems (Site Built Windows) (includes site assembled fixed windows only, does <u>not</u> include operable windows)				Unlabeled Skylight with Curb (includes glass/plastic, flat/domed, fixed/operable)				Unlabeled Skylight without Curb (includes glass/plastic, flat/domed, fixed/operable)		
Frame Type		Aluminum without Thermal Break	Aluminum with Thermal Break	Wood/Vinyl	Structural Glazing	Aluminum without Thermal Break	Aluminum with Thermal Break	Reinforced Vinyl/ Aluminum Clad Wood	Wood/Vinyl	Aluminum without Thermal Break	Aluminum with Thermal Break	Structural Glazing
ID	Glazing Type											
	Single Glazing											
1	1/8" glass	1.22	1.11	0.98	1.11	1.98	1.89	1.75	1.47	1.36	1.25	1.25
2	1/4" acrylic/polycarb	1.08	0.96	0.84	0.96	1.82	1.73	1.60	1.31	1.21	1.10	1.10
3	1/8" acrylic/polycarb	1.15	1.04	0.91	1.04	1.90	1.81	1.68	1.39	1.29	1.18	1.18
	Double Glazing											
4	1/4" airspace	0.79	0.68	0.56	0.63	1.31	1.11	1.05	0.84	0.82	0.70	0.66
5	1/2" airspace	0.73	0.62	0.50	0.57	1.30	1.10	1.04	0.84	0.81	0.69	0.65
6	1/4" argon space	0.75	0.64	0.52	0.60	1.27	1.07	1.00	0.80	0.77	0.66	0.62
7	1/2" argon space	0.70	0.59	0.48	0.55	1.27	1.07	1.00	0.80	0.77	0.66	0.62
	Double Glazing, e=0.60 on surface 2 or 3											
8	1/4" airspace	0.76	0.65	0.53	0.61	1.27	1.08	1.01	0.81	0.78	0.67	0.63
9	1/2" airspace	0.69	0.58	0.47	0.54	1.27	1.07	1.00	0.80	0.77	0.66	0.62
10	1/4" argon space	0.72	0.61	0.49	0.56	1.23	1.03	0.97	0.76	0.74	0.63	0.58
11	1/2" argon space	0.67	0.56	0.44	0.51	1.23	1.03	0.97	0.76	0.74	0.63	0.58
	Double Glazing, e=0.40 on surface 2 or 3											
12	1/4" airspace	0.74	0.63	0.51	0.58	1.25	1.05	0.99	0.78	0.76	0.64	0.60
13	1/2" airspace	0.66	0.55	0.44	0.51	1.24	1.04	0.98	0.77	0.75	0.64	0.59
14	1/4" argon space	0.69	0.57	0.46	0.53	1.18	0.99	0.92	0.72	0.70	0.58	0.54
15	1/2" argon space	0.63	0.51	0.40	0.47	1.20	1.00	0.94	0.74	0.71	0.60	0.56
	Double Glazing, e=0.20 on surface 2 or 3											
16	1/4" airspace	0.70	0.59	0.48	0.55	1.20	1.00	0.94	0.74	0.71	0.60	0.56
17	1/2" airspace	0.62	0.51	0.39	0.46	1.20	1.00	0.94	0.74	0.71	0.60	0.56
18	1/4" argon space	0.64	0.53	0.42	0.49	1.14	0.94	0.88	0.68	0.65	0.54	0.50
19	1/2" argon space	0.57	0.46	0.35	0.42	1.15	0.95	0.89	0.68	0.66	0.55	0.51
	Double Glazing, e=0.10 on surface 2 or 3											
20	1/4" airspace	0.68	0.57	0.45	0.52	1.18	0.99	0.92	0.72	0.70	0.58	0.54

Product Type		Vertical Installation				Sloped Installation						
		Unlabeled Glazed Wall Systems (Site Built Windows) (includes site assembled fixed windows only, does <u>not</u> include operable windows)				Unlabeled Skylight with Curb (includes glass/plastic, flat/domed, fixed/operable)				Unlabeled Skylight without Curb (includes glass/plastic, flat/domed, fixed/operable)		
Frame Type		Aluminum without Thermal Break	Aluminum with Thermal Break	Wood/Vinyl	Structural Glazing	Aluminum without Thermal Break	Aluminum with Thermal Break	Reinforced Vinyl/ Aluminum Clad Wood	Wood/Vinyl	Aluminum without Thermal Break	Aluminum with Thermal Break	Structural Glazing
21	1/2" airspace	0.59	0.48	0.37	0.44	1.18	0.99	0.92	0.72	0.70	0.58	0.54
22	1/4" argon space	0.62	0.51	0.39	0.46	1.11	0.91	0.85	0.65	0.63	0.52	0.47
23	1/2" argon space	0.55	0.44	0.33	0.39	1.13	0.93	0.87	0.67	0.65	0.53	0.49
Double Glazing, e=0.05 on surface 2 or 3												
24	1/4" airspace	0.67	0.56	0.44	0.51	1.17	0.97	0.91	0.70	0.68	0.57	0.52
25	1/2" airspace	0.57	0.46	0.35	0.42	1.17	0.98	0.91	0.71	0.69	0.58	0.53
26	1/4" argon space	0.60	0.49	0.38	0.44	1.09	0.89	0.83	0.63	0.61	0.50	0.45
27	1/2" argon space	0.53	0.42	0.31	0.38	1.11	0.91	0.85	0.65	0.63	0.52	0.47
Triple Glazing												
28	1/4" airspaces	0.63	0.52	0.41	0.47	1.12	0.89	0.84	0.64	0.64	0.53	0.48
29	1/2" airspaces	0.57	0.46	0.35	0.41	1.10	0.87	0.81	0.61	0.62	0.51	0.45
30	1/4" argon spaces	0.60	0.49	0.38	0.43	1.09	0.86	0.80	0.60	0.61	0.50	0.44
31	1/2" argon spaces	0.55	0.45	0.34	0.39	1.07	0.84	0.79	0.59	0.59	0.48	0.42
Triple Glazing, e=0.20 on surface 2,3,4, or 5												
32	1/4" airspaces	0.59	0.48	0.37	0.42	1.08	0.85	0.79	0.59	0.60	0.49	0.43
33	1/2" airspaces	0.52	0.41	0.30	0.35	1.05	0.82	0.77	0.57	0.57	0.46	0.41
34	1/4" argon spaces	0.54	0.44	0.33	0.38	1.02	0.79	0.74	0.54	0.55	0.44	0.38
35	1/2" argon spaces	0.49	0.38	0.28	0.33	1.01	0.78	0.73	0.53	0.54	0.43	0.37
Triple Glazing, e=0.20 on surfaces 2 or 3 and 4 or 5												
36	1/4" airspaces	0.55	0.45	0.34	0.39	1.03	0.80	0.75	0.55	0.56	0.45	0.39
37	1/2" airspaces	0.48	0.37	0.26	0.31	1.01	0.78	0.73	0.53	0.54	0.43	0.37
38	1/4" argon spaces	0.50	0.39	0.29	0.34	0.99	0.75	0.70	0.50	0.51	0.40	0.35
39	1/2" argon spaces	0.45	0.34	0.24	0.29	0.97	0.74	0.69	0.49	0.50	0.39	0.33
Triple Glazing, e=0.10 on surfaces 2 or 3 and 4 or 5												
40	1/4" airspaces	0.54	0.43	0.32	0.37	1.01	0.78	0.73	0.53	0.54	0.43	0.37
41	1/2" airspaces	0.46	0.35	0.25	0.29	0.99	0.76	0.71	0.51	0.52	0.41	0.36
42	1/4" argon spaces	0.48	0.38	0.27	0.32	0.96	0.73	0.68	0.48	0.49	0.38	0.32
43	1/2" argon spaces	0.42	0.32	0.21	0.26	0.95	0.72	0.67	0.47	0.48	0.37	0.31
Quadruple Glazing, e=0.10 on surfaces 2 or 3 and 4 or 5												

Product Type		Vertical Installation				Sloped Installation						
		Unlabeled Glazed Wall Systems (Site Built Windows) (includes site assembled fixed windows only, does <u>not</u> include operable windows)				Unlabeled Skylight with Curb (includes glass/plastic, flat/domed, fixed/operable)				Unlabeled Skylight without Curb (includes glass/plastic, flat/domed, fixed/operable)		
Frame Type		Aluminum without Thermal Break	Aluminum with Thermal Break	Wood/Vinyl	Structural Glazing	Aluminum without Thermal Break	Aluminum with Thermal Break	Reinforced Vinyl/ Aluminum Clad Wood	Wood/Vinyl	Aluminum without Thermal Break	Aluminum with Thermal Break	Structural Glazing
44	1/4" airspaces	0.49	0.38	0.28	0.33	0.97	0.74	0.69	0.49	0.50	0.39	0.33
45	1/2" airspaces	0.43	0.32	0.22	0.27	0.94	0.71	0.66	0.46	0.47	0.36	0.30
46	1/4" argon spaces	0.45	0.34	0.24	0.29	0.93	0.70	0.65	0.45	0.46	0.35	0.30
47	1/2" argon spaces	0.41	0.30	0.20	0.24	0.91	0.68	0.63	0.43	0.44	0.33	0.28
48	1/4" krypton spaces	0.41	0.30	0.20	0.24	0.88	0.65	0.60	0.40	0.42	0.31	0.25

## **NONRESIDENTIAL ACM MANUAL APPENDIX NJ**

# **Appendix NJ - Acceptance Requirements for Nonresidential Buildings**

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### ***NJ.1 Purpose and Scope***

ACM NJ defines acceptance procedures that must be completed before credit can be claimed for certain compliance measures. The procedures apply to nonresidential, high-rise residential and hotel/motel buildings as defined by the California Energy Commission's Energy Efficiency Standards for Nonresidential Buildings.

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### ***NJ.2 Introduction***

Acceptance Requirements are defined as the application of targeted inspection checks and functional and performance testing conducted to determine whether specific building components, equipment, systems, and interfaces between systems conform to the criteria set forth in the Standards and to related construction documents (plans or specifications). Acceptance Requirements can effectively improve code compliance and help determine whether equipment meets operational goals and whether it should be adjusted to increase efficiency and effectiveness.

This section describes the process for completing the Acceptance Requirements. The steps include the following:

- Document plans showing sensor locations, devices, control sequences and notes,
- Review the installation, perform acceptance tests and document results, and
- Document the operating and maintenance information, complete installation certificate and indicate test results on the Certificate of Acceptance, and submit the Certificate to the building department prior to receive a final occupancy permit.

Acceptance testing is not intended to take the place of commissioning or test and balance procedures that a building owner might incorporate into a building project. It is an adjunct process focusing only on demonstrating compliance with the Standards.

The installing contractor, engineer of record or owners agent shall be responsible for reviewing the plans and specifications to assure they conform to the Acceptance Requirements. This is typically done prior to signing a Certificate of Compliance.

The installing contractor, engineer of record or owners agent shall be responsible for providing all necessary instrumentation, measurement and monitoring, and undertaking all required acceptance requirement procedures. They shall be responsible for correcting all performance deficiencies and again implementing the acceptance requirement procedures until all specified systems and equipment are performing in accordance with the Standards.

The installing contractor, engineer of record or owners agent shall be responsible for documenting the results of the acceptance requirement procedures including paper and electronic copies of all measurement and monitoring results. They shall be responsible for performing data analysis, calculation of performance indices and crosschecking results with the requirements of the Standard. They shall be responsible for issuing a Certificate of Acceptance. Building departments shall not release a final Certificate of Occupancy until a Certificate of Acceptance is submitted that demonstrates that the specified systems and equipment have been shown to be performing in accordance with the Standards. The installing contractor, engineer of record or owners agent upon completion of undertaking all required acceptance requirement procedures shall record their State of California

Contractor's License number or their State of California Professional Registration License Number on each Certificate of Acceptance that they issue.

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### **NJ.3 Outdoor Air**

#### **NJ.3.1 Variable Air Volume Systems Outdoor Air Acceptance**

##### **NJ.3.1.1 Construction Inspection**

Prior to Acceptance Testing, verify and document the following:

- Outside air flow station is calibrated *OR* a calibration curve of outside air vs. outside air damper position, inlet vane signal, or VFD signal was completed during system TAB procedures.

##### **NJ.3.1.2 Equipment Testing**

Step 1: If the system has an outdoor air economizer, force the economizer high limit to disable economizer control (e.g. for a fixed drybulb high limit, lower the setpoint below the current outdoor air temperature)

Step 2: Drive all VAV boxes to the greater of the minimum airflow or 30% of the total design airflow. Verify and document the following:

- Measured outside airflow CFM corresponds to no less than 90% of the total value found on the Standards Mechanical Plan Check document MECH-3, Column H or Column I (which ever is greater).
- System operation stabilizes within 15 minutes after test procedures are initiated (no hunting).

Step 3: Drive all VAV boxes to achieve design airflow. Verify and document the following:

- Measured outside airflow CFM corresponds to no less than 90% of the total value found on Standards Mechanical Plan Check document MECH-3, Column H or Column I (which ever is greater).
- System operation stabilizes within 15 minutes after test procedures are initiated (no hunting).

#### **NJ.3.2 Constant Volume System Outdoor Air Acceptance**

##### **NJ.3.2.1 Construction Inspection**

Prior to Acceptance Testing, verify and document the following:

- The system has a fixed or motorized minimum outdoor air damper, or an economizer capable of maintaining a minimum outdoor air damper position.

##### **NJ.3.2.2 Equipment Testing**

Step 1: If the system has an outdoor air economizer, force the economizer high limit to disable economizer control (e.g. for a fixed drybulb high limit, lower the setpoint below the current outdoor air temperature)

- Measured outside airflow CFM with damper at minimum position corresponds to no less than 90% of the total value found on the Standards Mechanical Plan Check document MECH-3, Column H or Column I (which ever is greater).

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### **NJ.4 Packaged HVAC Systems**

Acceptance requirements apply only to constant volume, direct expansion (DX) packaged systems with gas furnaces or heat pumps.

## **NJ.4.1 Constant Volume Packaged HVAC Systems Acceptance**

### ***NJ.4.1.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Thermostat is located within the zone that the HVAC system serves.
- Space temperature thermostat is factory-calibrated (proof required) or field-calibrated.
- Appropriate temperature deadband has been programmed.
- Appropriate occupied, unoccupied, and holiday schedules have been programmed.
- Appropriate pre-occupancy purge has been programmed per Standards Section 121(c)2.
- Economizer lockout control sensor, if applicable, is factory-calibrated (proof required) or field-calibrated and setpoint properly set (refer to the *ECONOMIZERS* acceptance requirements section for detail).
- Demand control ventilation controller, if applicable, is factory-calibrated (proof required) or field-calibrated and setpoint properly set (refer to the *DEMAND CONTROL VENTILATION* acceptance requirements section for detail).

### ***NJ.4.1.2 Equipment Testing***

Step 1: Simulate heating load during occupied condition (e.g. by setting time schedule to include actual time and placing thermostat heating setpoint above actual temperature). Verify and document the following:

- Supply fan operates continually during occupied condition.
- Gas-fired furnace, heat pump or electric heater, if applicable, stages on.
- No cooling is provided by the unit.
- Outside air damper is open to the minimum position.

Step 2: Simulate “no-load” during occupied condition (e.g. by setting time schedule to include actual time and placing thermostat heating setpoints below actual temperature and cooling setpoint below actual temperature). Verify and document the following:

- Supply fan operates continually during occupied condition.
- Neither heating or cooling is provided by the unit.
- Outside air damper is open to the minimum position.

Step 3: If there is an economizer, simulate cooling load and economizer operation, if applicable, during occupied condition (e.g. by setting time schedule to include actual time and placing thermostat cooling setpoint below actual temperature). Verify and document the following:

- Supply fan operates continually during occupied condition.
- Refer to the *ECONOMIZERS* acceptance requirements section for testing protocols.
  - No heating is provided by the unit.

Step 4: If there is no economizer, simulate cooling load during occupied condition (e.g. by setting time schedule to include actual time and placing thermostat cooling setpoint below actual temperature). Verify and document the following:

- Supply fan operates continually during occupied condition.
- Compressor(s) stage on.
- No heating is provided by the unit.

- Outside air damper is open to the minimum position.

Step 5: Change the time schedule force the unit into unoccupied mode. Verify and document the following:

- Supply fan turns off.
- Outside air damper closes completely.

Step 6: Simulate heating load during setback conditions (e.g. by setting time schedule to exclude actual time and placing thermostat setback heating setpoint above actual temperature). Verify and document the following:

- Supply fan cycles on.
- Gas-fired furnace, heat pump or electric heater, if applicable, stages on.
- No cooling is provided by the unit.
- Supply fan cycles off when heating equipment is disabled.

Step 7: If there is an economizer, simulate cooling load and economizer operation, if applicable, during unoccupied condition (e.g. by setting time schedule to exclude actual time and placing thermostat setup cooling setpoint below actual temperature). Verify and document the following:

- Supply fan cycles on.
- Refer to the *ECONOMIZERS* acceptance requirements section for testing protocols.
- Supply fan cycles off when call for cooling is satisfied (simulated by lowering the thermostat setpoint to below actual temperature).
- Outside air damper closes when unit cycles off.

Step 8: If there is no economizer, simulate cooling load during setup condition (e.g. by setting time schedule to exclude actual time and placing thermostat setup cooling setpoint above actual temperature). Verify and document the following:

- Supply fan cycles on.
- Compressor(s) stage on to satisfy cooling space temperature setpoint.
- No heating is provided by the unit.
- Supply fan cycles off when cooling equipment is disabled.

Step 9: Simulate manual override during unoccupied condition (e.g. by setting time schedule to exclude actual time or by pressing override button). Verify and document the following:

- System reverts to “occupied” mode and operates as described above to satisfy a heating, cooling, or no load condition.
- System turns off when manual override time period expires.

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## ***NJ.5. Air Distribution Systems***

Acceptance requirements apply only to systems covered by Section 144(k).

### **NJ.5.1 Air Distribution Acceptance**

#### ***NJ.5.1.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Drawbands are either stainless steel worm-drive hose clamps or UV-resistant nylon duct ties.

- Flexible ducts are not constricted in any way (for example pressing against immovable objects or squeezed through openings).
- Duct leakage tests shall be performed before access to ductwork and associated connections are blocked by permanently installed construction material.
- Joints and seams are not sealed with a cloth back rubber adhesive tape unless used in combination with mastic and drawbands.
- Duct R-values are verified.
- Insulation is protected from damage and suitable for outdoor service if applicable.

#### ***NJ.5.1.2 Equipment Testing***

Step 1: Perform duct leakage test per 2003 Nonresidential ACM Approved Manual, Appendix NG, Section 4.3.8.2. Certify the following:

- Duct leakage conforms to the requirements of Section 144(k)..

Step 2: Obtain HERS Rater field verification as required by Chapter 7 and Appendix NG.

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### ***NJ.6. Lighting Control Systems***

Lighting control testing is performed on:

- Manual Daylighting Controls.
- Automatic Daylighting Controls.
- Occupancy Sensors.
- Automatic Time-switch Control.

#### ***NJ.6.1 Automatic Daylighting Controls Acceptance***

##### ***NJ.6.1.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- All control devices (photocells) have been properly located, factory-calibrated (proof required) or field-calibrated and set for appropriate set points and threshold light levels.
- Installer has provided documentation of setpoints, setting and programming for each device.
- Luminaires located in either a horizontal daylit area(s) or a vertical daylit area(s) are powered by a separate lighting circuit from non-daylit areas.

##### ***NJ.6.1.2 Equipment Testing***

###### ***Continuous Dimming Control Systems***

Step 1: Simulate bright conditions for a continuous dimming control system. Verify and document the following:

- Lighting power reduction is at least 65% under fully dimmed conditions.
- At least one control step reduces the lighting power by at least 30%.
- Only luminaires in daylit zone are affected by daylight control.
- Automatic daylight control system reduces the amount of light delivered to the space uniformly.



- Dimming control system provides reduced flicker operation over the entire operating range per Standards Section 119(e)2.
- Lumen measurements in the space, location of measurements and specific device settings, program settings and other measurements are documented.

Step 2: Simulate dark conditions for a continuous dimming control system. Verify and document the following:

- Automatic daylight control system increases the amount of light delivered to the space uniformly.
- Dimming control system provides reduced flicker operation over the entire operating range per Standards Section 119(e)2.
- Lumen measurements in the space, location of measurements and specific device settings, program settings and other measurements are documented.

#### *Stepped Dimming Control Systems*

Step 1: Simulate bright conditions for a stepped dimming control system. Verify and document the following:

- Lighting power reduction is at least 50% under fully dimmed conditions.
- Only luminaires in daylit zone are affected by daylight control.
- Automatic daylight control system reduces the amount of light delivered to the space relatively uniformly as per Section 131(b).
- Automatic daylight control system reduces the amount of light delivered to the space per manufacturer's specifications for power level versus light level.
- Minimum time delay between step changes is 3 minutes to prevent short cycling.
- Lumen measurements in the space, location of measurements and specific device settings, program settings and other measurements are documented.

Step 2: Simulate dark conditions for a stepped dimming control system. Verify and document the following:

- Automatic daylight control system increases the amount of light delivered to the space per manufacturer's specifications for power level versus light level.
- Stepped dimming control system provides reduced flicker over the entire operating range per Standards Section 119(e)2.
- Minimum time delay between step changes is 3 minutes to prevent short cycling.
- Lumen measurements in the space, location of measurements and specific device settings, program settings and other measurements are documented.

#### *Stepped Switching Control Systems*

Step 1: Simulate bright conditions for a stepped switching control system. Verify and document the following:

- Lighting power reduction is at least 50% under fully switched conditions per Standards Section 119(e)1.
- Only luminaires in daylit zone are affected by daylight control.
- Automatic daylight control system reduces the amount of light delivered to the space relatively uniformly as per Section 131(b).
- Automatic daylight control system reduces the amount of light delivered to the space per manufacturer's specifications for power level versus light level.
- Single- or multiple-stepped switching controls provide a dead band of at least three minutes between switching thresholds to prevent short cycling.

- Lumen measurements in the space, location of measurements and specific device settings, program settings and other measurements are documented.

Step 2: Simulate dark conditions for a stepped switching control system. Verify and document the following:

- Automatic daylight control system increases the amount of light delivered to the space per manufacturer's specifications for power level verses light level.
- Single- or multiple-stepped switching controls provide a dead band of at least three minutes between switching thresholds to prevent short cycling.
- Lumen measurements in the space, location of measurements and specific device settings, program settings and other measurements are documented.

## **NJ.6.2 Occupancy Sensor Acceptance**

### ***NJ.6.2.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Occupancy sensor has been located to minimize false signals.
- Occupancy sensors do not encounter any obstructions that could adversely affect desired performance.
- Ultrasound occupancy sensors do not emit audible sound.

### ***NJ.6.2.2 Equipment Testing***

Step 1: For a representative sample of building spaces, simulate an unoccupied condition. Verify and document the following:

- Lights controlled by occupancy sensors turn off within a maximum of 30 minutes from the start of an unoccupied condition per Standard Section 119(d).
- The occupant sensor does not trigger a false "on" from movement in an area adjacent to the controlled space or from HVAC operation.
- Signal sensitivity is adequate to achieve desired control.

Step 2: For a representative sample of building spaces, simulate an occupied condition. Verify and document the following:

- Status indicator or annunciator operates correctly.
- Lights controlled by occupancy sensors turn on immediately upon an occupied condition, *OR* sensor indicates space is "occupied" and lights are turned on manually (automatic OFF and manual ON control strategy).

## **NJ.6.3 Manual Daylighting Controls Acceptance**

### ***NJ.6.3.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- If dimming ballasts are specified for light fixtures within the daylit area, make sure they meet all the Standards requirements, including "reduced flicker operation" for manual dimming control systems.

### ***NJ.6.3.2 Equipment Testing***

Step 1: Perform manual switching control. Verify and document the following:

- Manual switching or dimming achieves a lighting power reduction of at least 50%.

- The amount of light delivered to the space is uniformly reduced.

## **NJ.6.4 Automatic Time Switch Control Acceptance**

### ***NJ.6.4.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Automatic time switch control is programmed with acceptable weekday, weekend, and holiday (if applicable) schedules.
- Document for the owner automatic time switch programming including weekday, weekend, holiday schedules as well as all set-up and preference program settings.
- Verify the correct time and date is properly set in the time switch.
- Verify the battery is installed and energized.
- Override time limit is no more than 2 hours.

### ***NJ.6.4.2 Equipment Testing***

Step 1: Simulate occupied condition. Verify and document the following:

- All lights can be turned on and off by their respective area control switch.
- Verify the switch only operates lighting in the ceiling-height partitioned area in which the switch is located.

Step 2: Simulate unoccupied condition. Verify and document the following:

- All non-exempt lighting turn off per Section 131 (d)1.
- Manual override switch allows only the lights in the selected ceiling height partitioned space where the override switch is located, to turn on or remain on until the next scheduled shut off occurs.
- All non-exempt lighting turns off.

---

## ***NJ.7. Air Economizer Controls***

Economizer testing is performed on all built-up systems and on packaged systems per Standards Section 144 (e)1. Air economizers installed by the HVAC system manufacturer and certified to the commission as being factory calibrated and tested do not require field testing.

### **NJ.7.1 Economizer Acceptance**

#### ***NJ.7.1.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Economizer lockout setpoint complies with Table 144-C per Standards Section 144 (e) 3.
- System controls are wired correctly to ensure economizer is fully integrated (i.e. economizer will operate when mechanical cooling is enabled).
- Economizer lockout control sensor location is adequate (open to air but not exposed to direct sunlight nor in an enclosure; away from sources of building exhaust; at least 25 feet away from cooling towers).
- Relief fan or return fan (if applicable) operates as necessary when the economizer is enabled to control building pressure.

- If no relief fan or return fan is installed, barometric relief dampers are installed to relieve building pressure when the economizer is operating.

### ***NJ.7.1.2 Equipment Testing***

Step 1: Simulate a cooling load and enable the economizer by adjusting the lockout control (fixed or differential dry-bulb or enthalpy sensor depending on system type) setpoint. Verify and document the following:

- Economizer damper modulates opens per Standards Section 144 (e)1A to maximum position to satisfy cooling space temperature setpoint.
- Return air damper modulates closed and is completely closed when economizer damper is 100% open.
- Economizer damper is 100% open before mechanical cooling is enabled.
- Relief fan or return fan (if applicable) is operating or barometric relief dampers freely swing open.
- Mechanical cooling is only enabled if cooling space temperature setpoint is not met with economizer at 100% open.
- Doors are not pushed ajar from over pressurization.

Step 2: Continue from Step 1 and disable the economizer by adjusting the lockout control (fixed or differential dry-bulb or enthalpy sensor depending on system type) setpoint. Verify and document the following:

- Economizer damper closes to minimum position.
- Return air damper opens to normal operating position.
- Relief fan (if applicable) shuts off or barometric relief dampers close. Return fan (if applicable) may still operate even when economizer is disabled.
- Mechanical cooling remains enabled until cooling space temperature setpoint is met.

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## ***NJ.8. Demand Control Ventilation (DCV) Systems***

Demand control ventilation is tested on package systems per Standards Section 121 (c)3.

### ***NJ.8.1 Packaged Systems DCV Acceptance***

#### ***NJ.8.1.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Carbon dioxide control sensor is factory calibrated (proof required) or field-calibrated with an accuracy of no less than 75 ppm.
- The sensor is located in the room between 1ft and 6 ft above the floor.
- System controls are wired correctly to ensure proper control of outdoor air damper system.

#### ***NJ.8.1.2 Equipment Testing***

Step 1: Simulate a high CO<sub>2</sub> load and enable the demand control ventilation by adjusting the demand control ventilation controller setpoint below ambient CO<sub>2</sub> levels. Verify and document the following:

- Outdoor air damper modulates opens per Standards to maximum position to satisfy outdoor air requirements specified in Section 121(c).

Step 2: Continue from Step 1 and disable demand control ventilation by adjusting the demand control ventilation controller setpoint above ambient CO<sub>2</sub> levels. Verify and document the following:

- Outdoor air damper closes to minimum position.

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## ***NJ.9. Variable Frequency Drive Systems***

### **NJ.9.1 Supply Fan Variable Flow Controls**

#### ***NJ.9.1.1 Construction Inspection***

Prior to Performance Testing, verify and document the following:

- Discharge static pressure sensor is factory calibrated (proof required) or field-calibrated with secondary source.
- Disable discharge static pressure reset sequences to prevent unwanted interaction while performing tests.

#### ***NJ.9.1.2 Equipment Testing***

Step 1: Drive all VAV boxes to achieve design airflow. Verify and document the following:

- Witness proper response from supply fan (e.g. VFD ramps up to full speed; inlet vanes open full).
- Supply fan maintains discharge static pressure within +/-10% of setpoint.
- Measured maximum airflow corresponds to design and/or TAB report within +/-10%.
- System operation stabilizes within a reasonable amount of time after test procedures are initiated (no hunting).

Step 2: Drive all VAV boxes to minimum flow or to achieve 30% total design airflow whichever is larger. Verify and document the following:

- Witness proper response from supply fan (VFD slows fan speed; inlet vanes close).
- Supply fan maintains discharge static pressure within +/-10% of setpoint.
- System operation stabilizes within a reasonable amount of time after test procedures are initiated (no hunting).

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## ***NJ.10. Hydronic System Controls Acceptance***

Hydronic controls Acceptance Testing will be performed on:

- Variable Flow Controls
- Automatic Isolation Controls
- Supply Water Temperature Reset Controls
- Water-loop Heat Pump Controls
- Variable Frequency Drive Control

**NJ.10.1 Variable Flow Controls*****NJ.10.1.1 Construction Inspection***

Prior to Acceptance Testing, verify and document the following:

- Valve and piping arrangements were installed per the design drawings to achieve flow reduction requirements.
- Installed valve and hydronic connection pressure ratings meet specifications.
- Installed valve actuator torque characteristics meet specifications.

***NJ.10.1.2 Equipment Testing***

Step 1: Open all control valves. Verify and document the following:

- System operation achieves design conditions.

Step 2: Initiate closure of control valves. Verify and document the following:

- The design pump flow control strategy achieves flow reduction requirements.
- Ensure all valves operate correctly against the minimum flow system pressure condition.

**NJ.10.2 Automatic Isolation Controls*****NJ.10.2.1 Construction Inspection***

Prior to Acceptance Testing, verify and document the following:

- Valve and piping arrangements were installed per the design drawings to achieve equipment isolation requirements.
- Installed valve and hydronic connection pressure ratings meet specifications.
- Installed valve actuator torque characteristics meet specifications.

***NJ.10.2.2 Equipment Testing***

Step 1: Open all control valves. Verify and document the following:

- System operation achieves design conditions.

Step 2: Initiate shut-down sequence on individual pieces of equipment. Verify and document the following:

- The design control strategy meets isolation requirements automatically upon equipment shut-down.
- Ensure all valves operate correctly at shut-off system pressure conditions.

### **NJ.10.3 Supply Water Temperature Reset Controls**

#### ***NJ.10.3.1 Construction Inspection***

Prior to Acceptance Testing, verify and document the following:

- ALL SENSORS HAVE BEEN CALIBRATED.
- Sensor locations are adequate to achieve accurate measurements.
- Installed sensors comply with specifications.

#### ***NJ.10.3.2 Equipment Testing***

Step 1: Manually change design control variable to maximum setpoint. Verify and document the following:

- Chilled or hot water temperature setpoint is reset to appropriate value.
- Actual supply temperature changes to meet setpoint.

Step 2: Manually change design control variable to minimum setpoint. Verify and document the following:

- Chilled or hot water temperature setpoint is reset to appropriate value.
- Actual supply temperature changes to meet setpoint.

### **NJ.10.4 Water-loop Heat Pump Controls**

#### ***NJ.10.4.1 Construction Inspection***

Prior to Acceptance Testing, verify and document the following:

- Valves were installed per the design drawings to achieve equipment isolation requirements.
- Installed valve and hydronic connection pressure ratings meet specifications.
- Installed valve actuator torque characteristics meet specifications.
- All sensor locations comply with design drawings.
- All sensors are calibrated.
- VFD minimum speed setpoint exceeds motor manufacturer's requirements.
- VFD minimum speed setpoint should not be set below the pumping energy curve inflection point (i.e. combination of pump-motor-VFD efficiency at reduced load may cause power requirements to increase upon further reduction in load).

#### ***NJ.10.4.2 Equipment Testing***

Step 1: Open all control valves. Verify and document the following:

- System operation achieves design conditions +/- 5%.

- VFD operates at 100% speed at full flow conditions.

Step 2: Initiate shut-down sequence on each individual heat pumps. Verify and document the following:

- Isolation valves close automatically upon unit shut-down.
- Ensure all valves operate correctly at shut-off system pressure conditions.
- Witness proper response from VFD (speed decreases as valves close).
- System operation stabilizes within 5 minutes after test procedures are initiated (no hunting).

Step 3: Adjust system operation to achieve 50% flow. Verify and document the following:

- VFD input power less than 30% of design.

Step 4: Adjust system operation to achieve a flow rate that would result in the VFD operating below minimum speed setpoint. Verify and document the following:

- Ensure VFD maintains minimum speed setpoint regardless of system flow operating point.

## **NJ.10.5 Variable Frequency Drive Controls**

### ***NJ.10.5.1 Construction Inspection***

Prior to Acceptance Testing, verify and document the following:

- All valves, sensors, and equipment were installed per the design drawings.
- All installed valves, sensors, and equipment meet specifications.
- All sensors are calibrated.
- VFD minimum speed setpoint exceeds motor manufacturer's requirements.
- VFD minimum speed setpoint should not be set below the pumping energy curve inflection point (i.e. combination of pump-motor-VFD efficiency characteristics at reduced load may cause input power to increase upon further reduction in load).

### ***NJ.10.5.2 Equipment Testing***

Step 1: Open all control valves. Verify and document the following:

- System operation achieves design conditions +/- 5%.
- VFD operates at 100% speed at full flow conditions.

Step 2: Modulate control valves closed. Verify and document the following:

- Ensure all valves operate correctly at system operating pressure conditions.
- Witness proper response from VFD (speed decreases as valves close).



- System operation stabilizes within 5 minutes after test procedures are initiated (no hunting).

Step 3: Adjust system operation to achieve 50% flow. Verify and document the following:

- VFD input power less than 30% of design.

Step 4: Adjust system operation to achieve a flow rate that would result in the VFD operating below minimum speed setpoint. Verify and document the following:

- Ensure VFD maintains minimum speed setpoint regardless of system flow operating point.